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Session ID: **ENG445**



# **ENG-445**

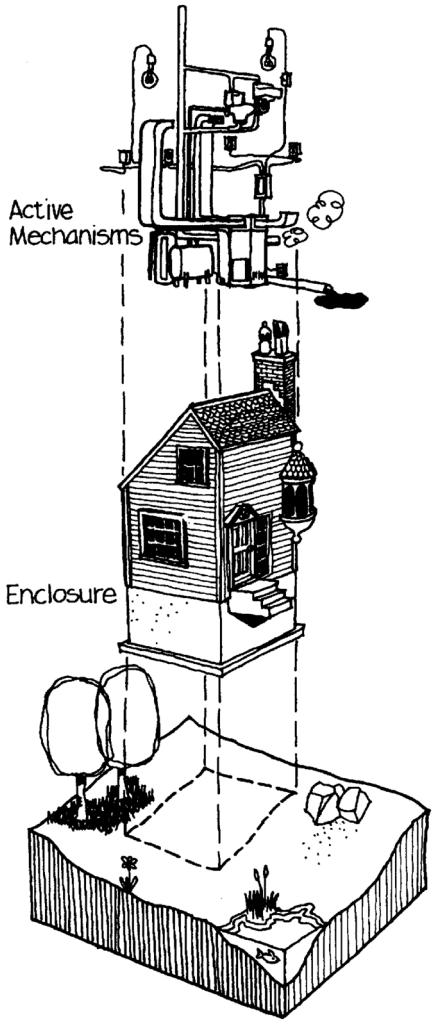
# **Building Energetics**

**Heating in Buildings –  
Emission Systems and  
Thermal Comfort**

**Dr. Jaafar YOUNES,  
Assist. Professor  
Dolaana Khovalyg**

21 November 2024

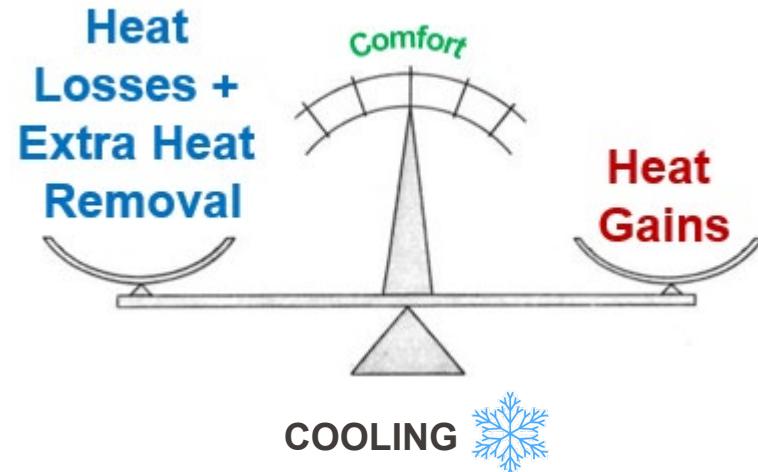
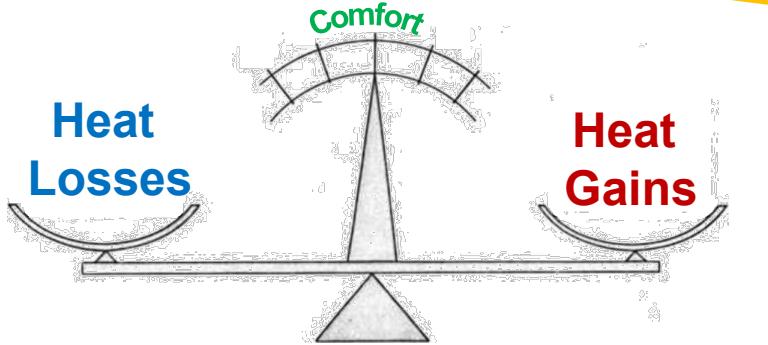
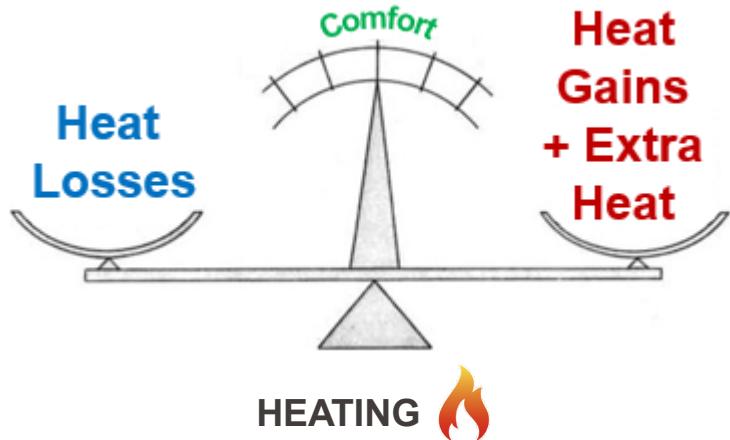
Week	Date	Topic	Timing	Teacher	Project (AS, MF)
9	07/11	Building envelope, thermal performance of building elements	45' x 2	DK	Tutorial building envelope
		Exercises			
10	14/11	Heating and cooling demand in buildings	45' x 2	DK	Free work
		Exercises			
11	21/11	Thermal systems for heating and their effect of human comfort	45' x 2	JY	Free work
		Exercises			
12	28/11	Thermal systems for cooling and their effect of human comfort	45' x 2	DK	Tutorial heating systems (emission systems)
		Exercises			



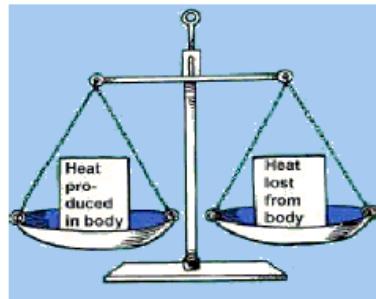
# CONTENT:

- **Introduction**
- **Overview of Emission Systems:**
  - Definition
  - All-air systems
  - Radiators (convectors)
  - Radiant systems
- **Technical Characteristics**
  - Local discomfort limits
  - Convectors vs. Embedded systems
- **Thermal Comfort vs. Emission Systems**
  - Comparative study overview
- **Standard References**
- **Summary**

- **Comfortable indoor temperature** is maintained by *balanced* heat losses and heat gains
- **Heating** or **cooling** is needed when they are *imbalanced* and **extra** heat addition or removal is necessary



- **Thermal neutrality** for the body as a whole is a necessary, but *not sufficient condition* for thermal comfort.
- **Local thermal discomfort** due to *draught, vertical temperature gradient, radiant asymmetry, or warm or cold floors* may cause occupants to find **the thermal conditions unacceptable**.



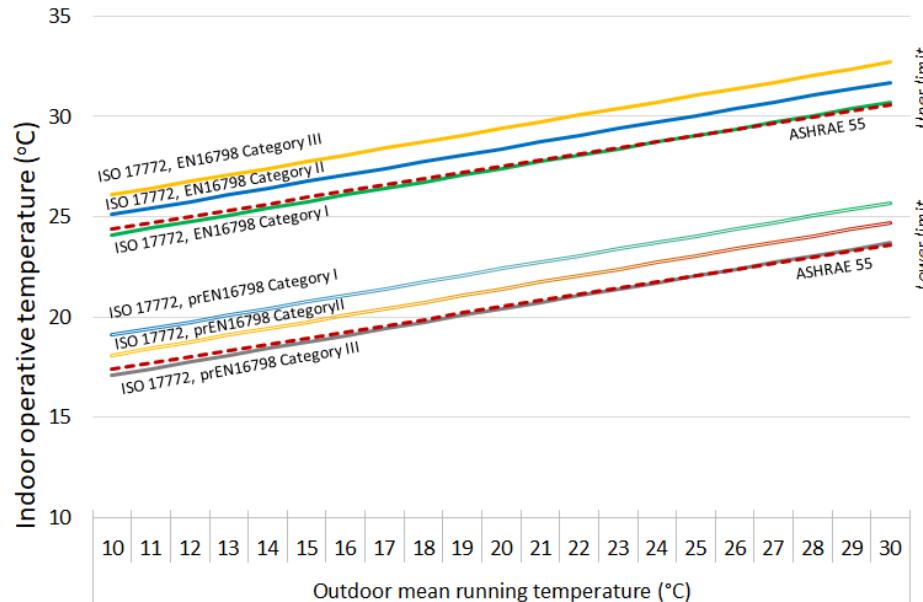
***It is essential to evaluate thermal comfort in 2 steps:***

- 1) Define the acceptable operative temperature
- 2) Check that there is no local discomfort

# Thermal Comfort: Adaptive Model

From Week 02

- Considers **thermal comfort** as a result of **adaptation** (physiological, behavioral, psychological)
- A *strong* relationship of the **comfortable temperatures** inside a building with the **mean temperatures prevailing outside** the building for *naturally ventilated* buildings (in 'free-running')



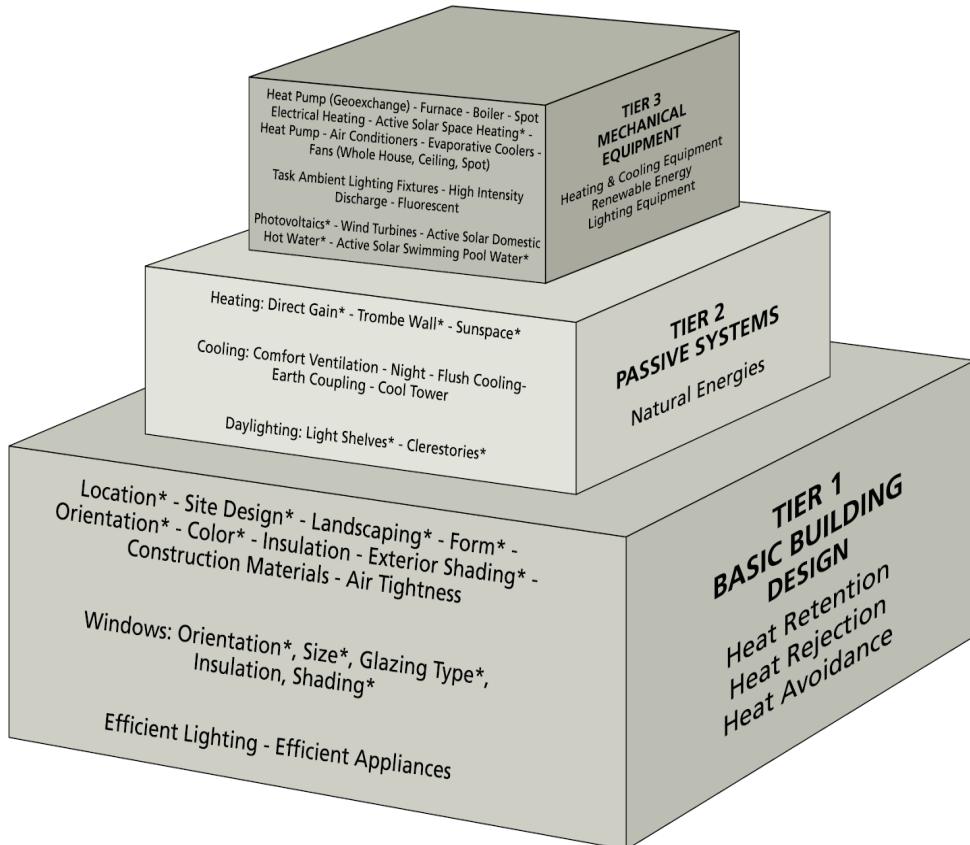
Standard	Categories	$T_{op}$ (°C), upper limit	$T_{op}$ (°C), lower limit	$T_{rm}$ (°C), applicability range
ISO 17772, EN 16798	I	$0.33*T_{rm}+20.8$	$0.33*T_{rm}+15.8$	10-30
	II	$0.33*T_{rm}+21.8$	$0.33*T_{rm}+14.8$	10-30
	III	$0.33*T_{rm}+22.8$	$0.33*T_{rm}+13.8$	10-30
ASHRAE 55	acceptable (80%)	$0.31*T_{rm}+21.3$	$0.31*T_{rm}+14.3$	10-33.5
	acceptable (90%)	$0.31*T_{rm}+21.3$	$0.31*T_{rm}+15.3$	

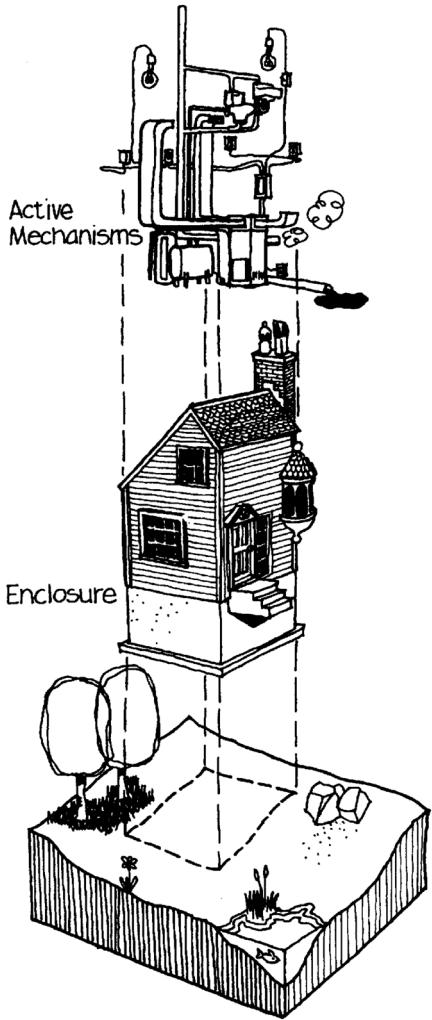
# Three-Tier Design Approach

From Week 10

Table 1.4A The Three-Tier Design Approach

	Heating	Cooling
Tier 1	Conservation	Heat avoidance
Basic Building Design	1. Surface-to-volume ratio 2. Insulation 3. Infiltration	1. Shading 2. Exterior colors 3. Insulation 4. Mass
Tier 2	Passive solar	Passive cooling
Natural Energies and Passive Techniques	1. Direct gain 2. Trombe wall 3. Sunspace	1. Evaporative cooling 2. Night-flush cooling 3. Comfort ventilation 4. Cool towers
Tier 3	Heating equipment	Cooling equipment
Mechanical and Electrical Equipment	1. Furnace 2. Boiler 3. Ducts/Pipes 4. Fuels	1. Refrigeration machine 2. Ducts 3. Geo-exchange





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## Active (mechanical) Heating/Cooling System

=

**1** Emission system  
(radiators, fan coils, etc.)

+

**2** Distribution system  
(pipe work, ducts, circulation pumps)

+

**3** Storage  
(water tanks, etc.)

+

**4** Generation system  
(heat pump, boiler, etc.)

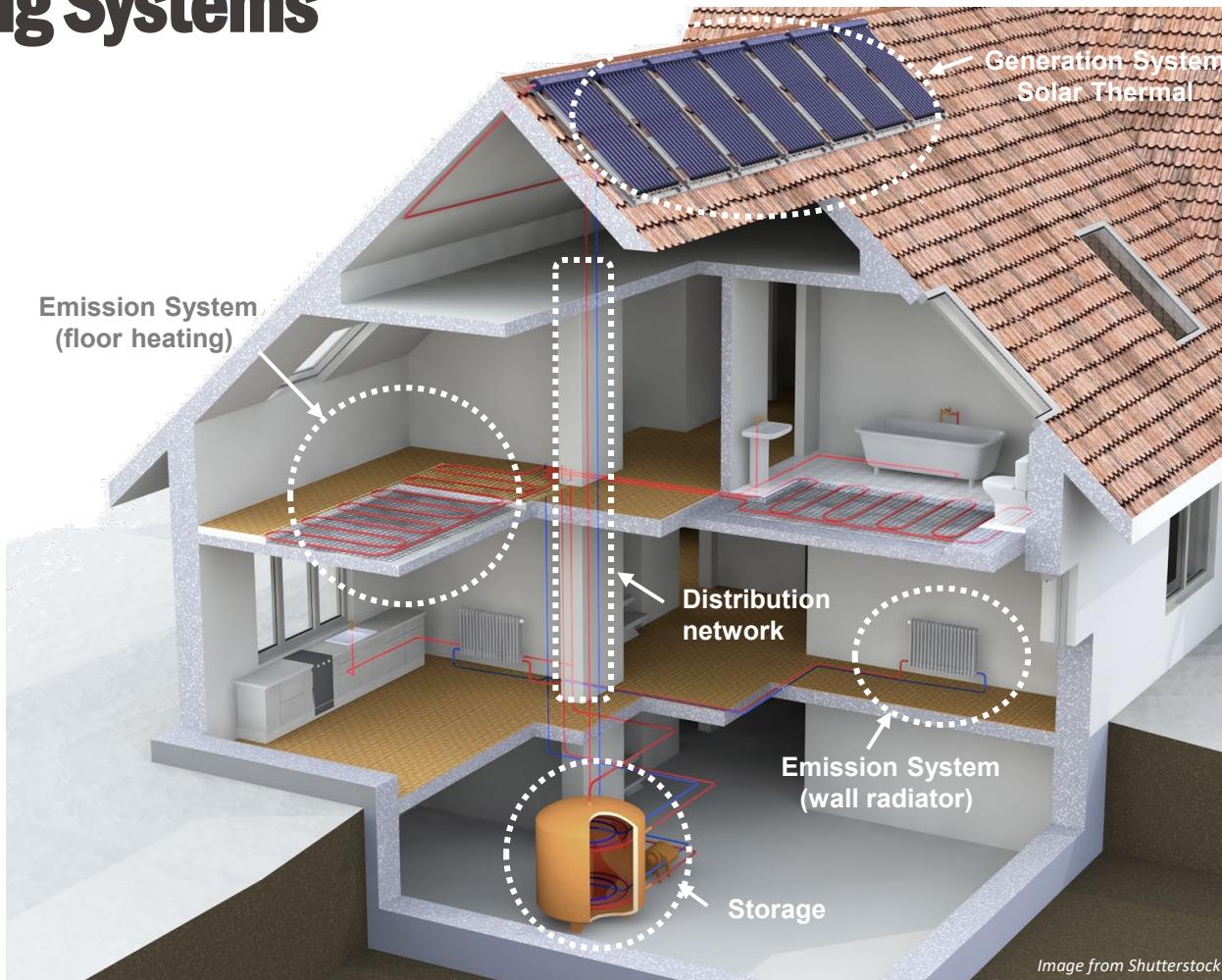
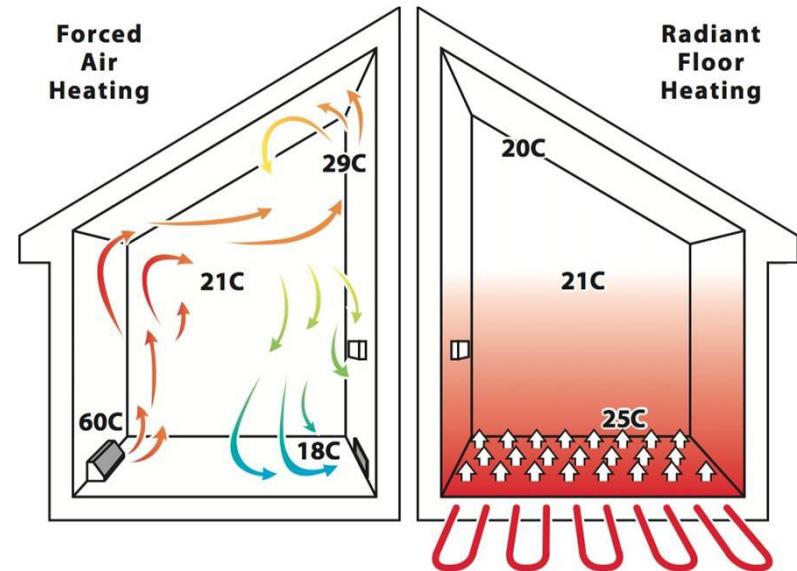
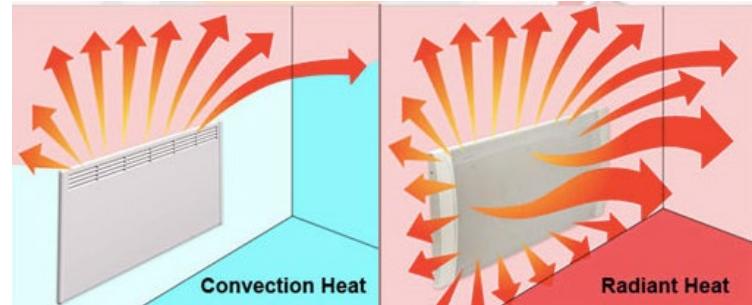


Image from Shutterstock

- Multiple ways to name - *indoor emission systems*, *indoor terminal units*, ..
- **Building elements** that use different heat transfer mechanisms and media to *emit* and *remove heat* and/or *moisture* from indoor spaces
- They differ in their capabilities of *addressing*:
  - sensible and latent loads
  - methods of **heat emission or removal**: convection, radiation, combined
  - maximum heating/cooling capacities
  - medium of **energy distribution** (i.e., heat carrier) – water, air, electricity
  - *local* or *total volume conditioning* (for convective systems)



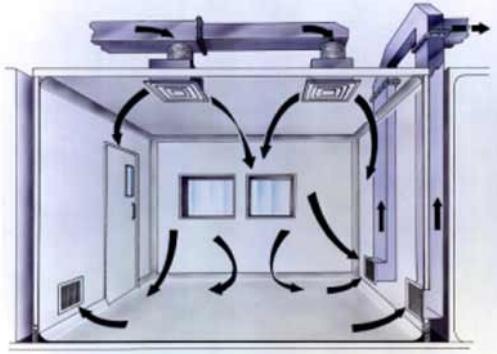
<https://airflow.ie/underfloor-heating/>



## All-Air Systems

**centralized** air conditioning

heat extraction using: **air**



- Air supply through **grills** (no air deflection)



- Air supply through **diffusers** (diffuses air)



**localized** air conditioning

heat extraction using: **refrigerant, water**



**Fancoils, indoor units** (air recirculation)



**Chilled beams** (active and passive) thermal conditioning + fresh air supply (active only)

## Radiant systems

**centralized** water conditioning

heat extraction using: **water**



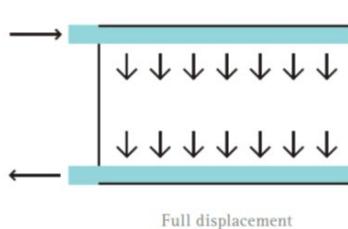
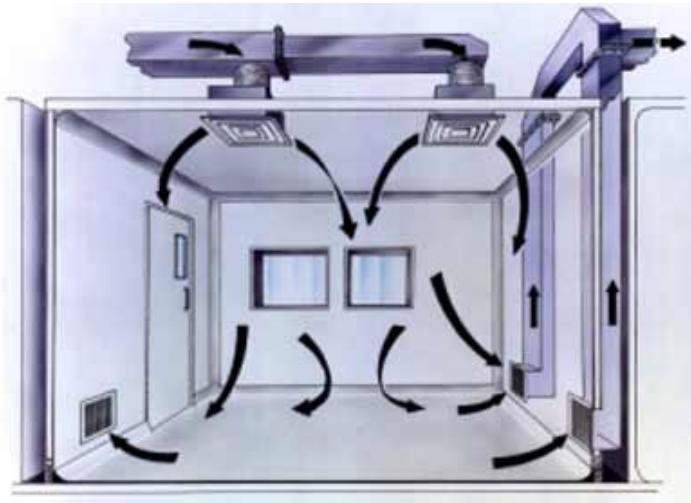
**Radiant ceiling**



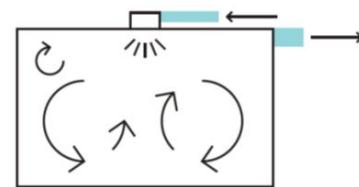
**Floor/Wall systems**

# Convective (All-Air) Systems

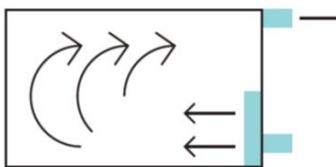
- A system where the **air** is used as **the heat carrier** (*medium of energy distribution*) and the **heat exchange** with **the conditioned space** is entirely by **convection**.
- Require **higher air flow rates than radiant systems** since **the entire heating/cooling load** needs to be addressed by the **ventilation system**
- **Types of systems:** mixing ventilation, displacement ventilation, underfloor air distribution, personalized ventilation, etc.
- Air can be **conditioned** in a **air-handling unit** using *various approaches* (electric heating, with hot water from a boiler or a heat pump, etc.)



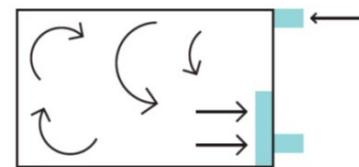
Full displacement



Full mixing

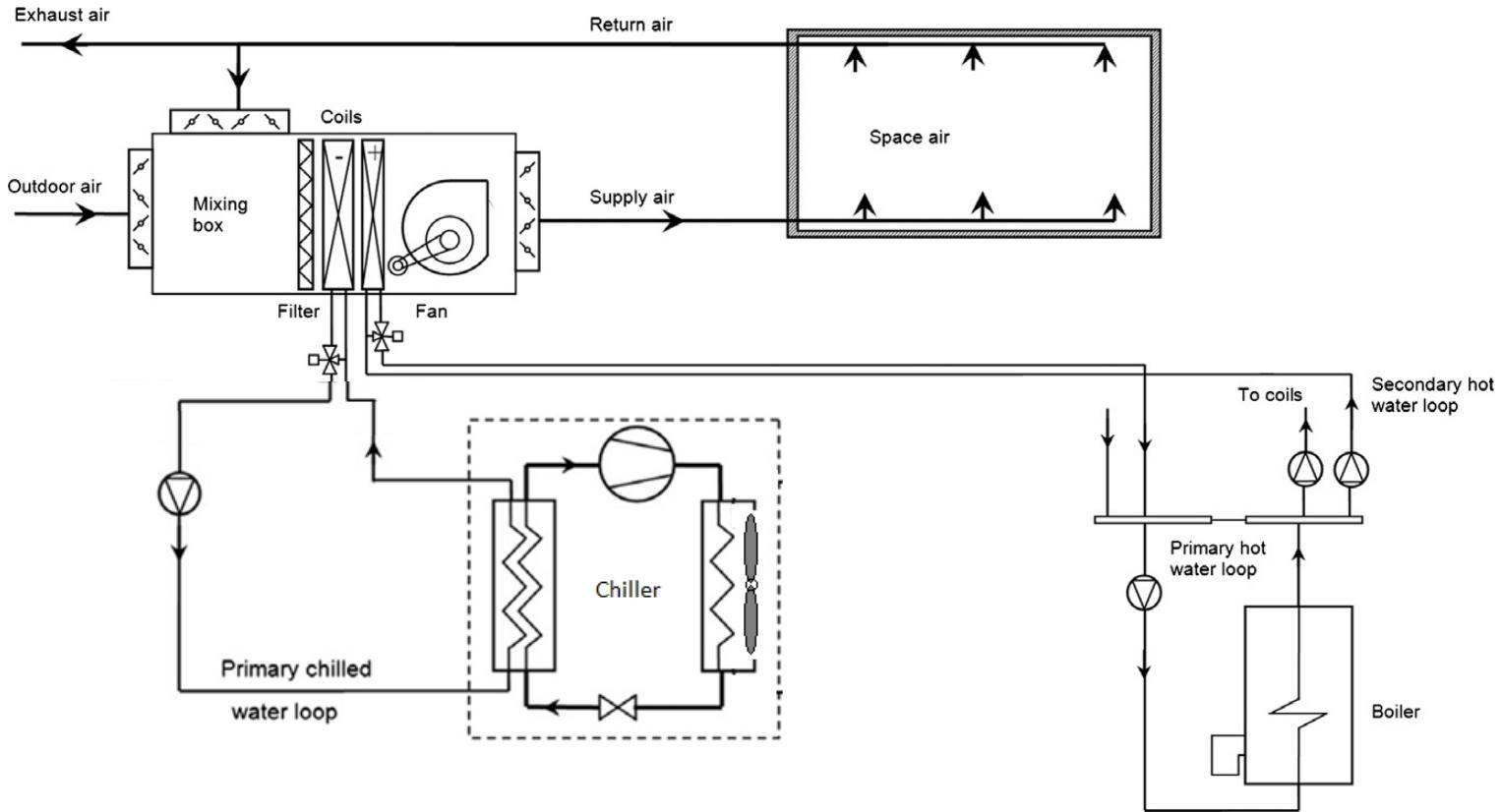


Local displacement

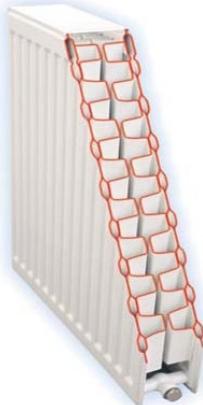


Local exhaust

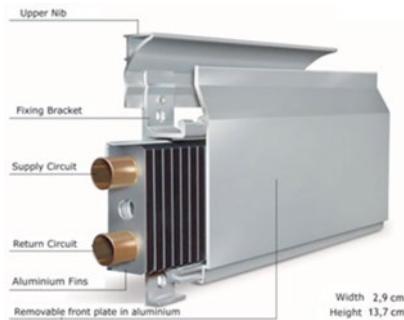
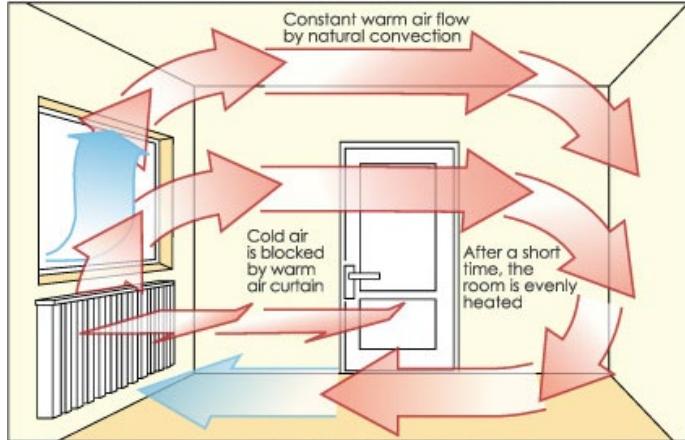
# Convective (All-Air) System: Supply Side



- The most conventional heating practice
- Types: **electric** or **water-heated** (hot water circulates through pipes)
- Heat transfer mainly by **natural convection**
- **Fins** are used to *increase* the heat transfer area
- The source of heat is *not directly exposed* due to aesthetic and **safety purposes**
- Configuration: horizontal, column, towel radiators, etc.



Skirting boards (electric and water-based)



Baseboard radiator

# Steam Radiators

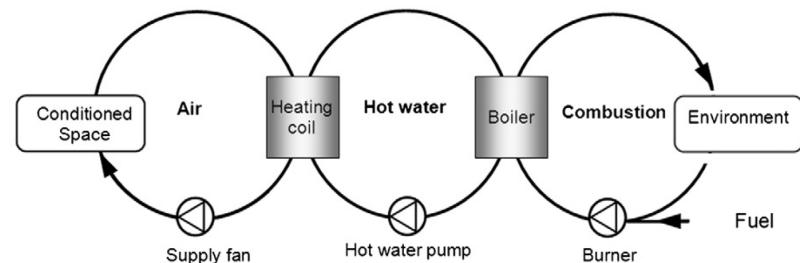
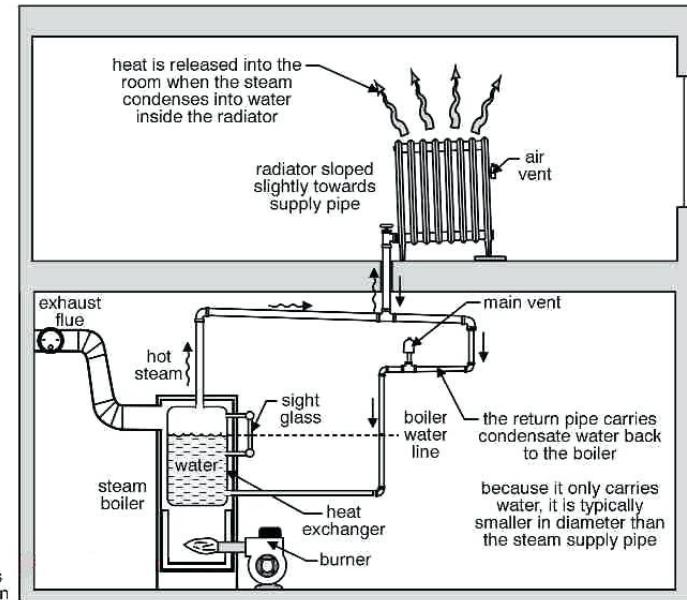
- One of the “oldest” heat emitting practices
- **1831**: AM Perkins (England) devised a high-pressure system of hot-water heating (steam at  $\sim 170^{\circ}\text{C}$  and pressure  $\sim 15$  atm)



Patent from 1867

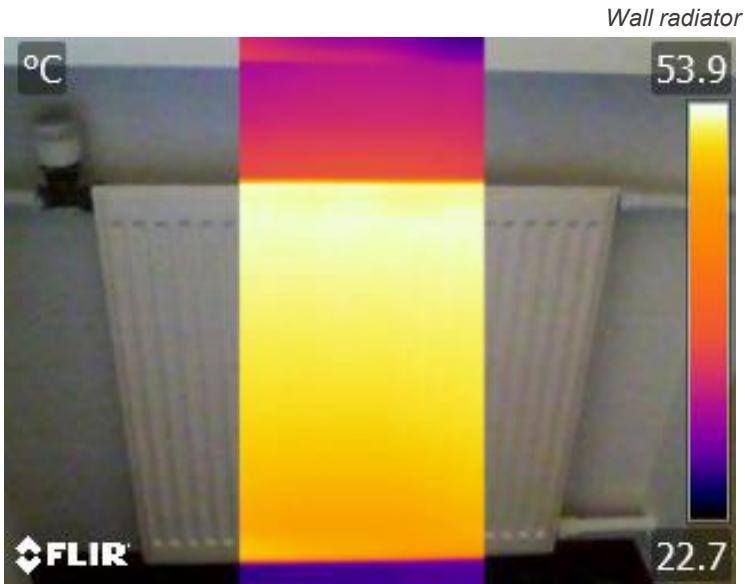


## How steam systems work



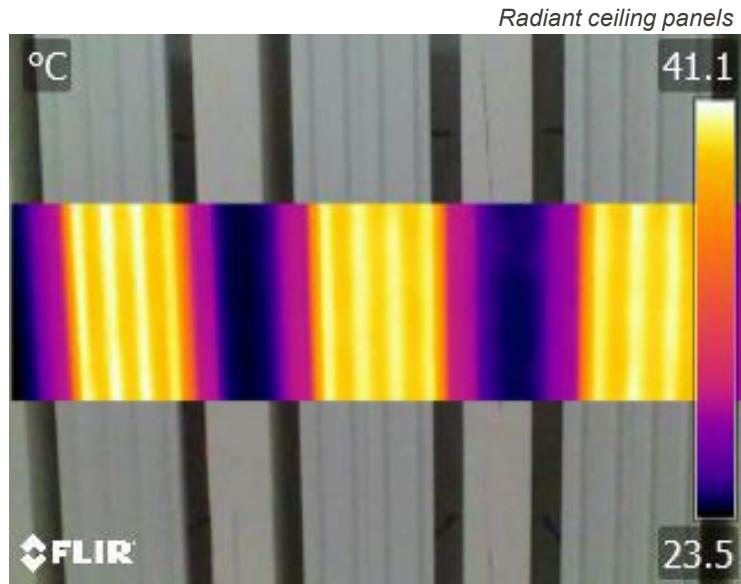
# Hydronic Radiant Systems

## “Steam” Radiators



- Small heat transfer area
- **Requires high water temperature ( $>50$  °C)**
- Needs to be coupled with **high temperature water generation system** (district heating, boilers)
- **Non-uniform** indoor thermal environment

## Radiant Systems



- **Large** heat transfer area
- **Low temperature heating (30-40 °C)**
- Better coupling with **water generation systems coupled with renewable sources (HPs, GHX)**
- Provides **uniform** indoor environment

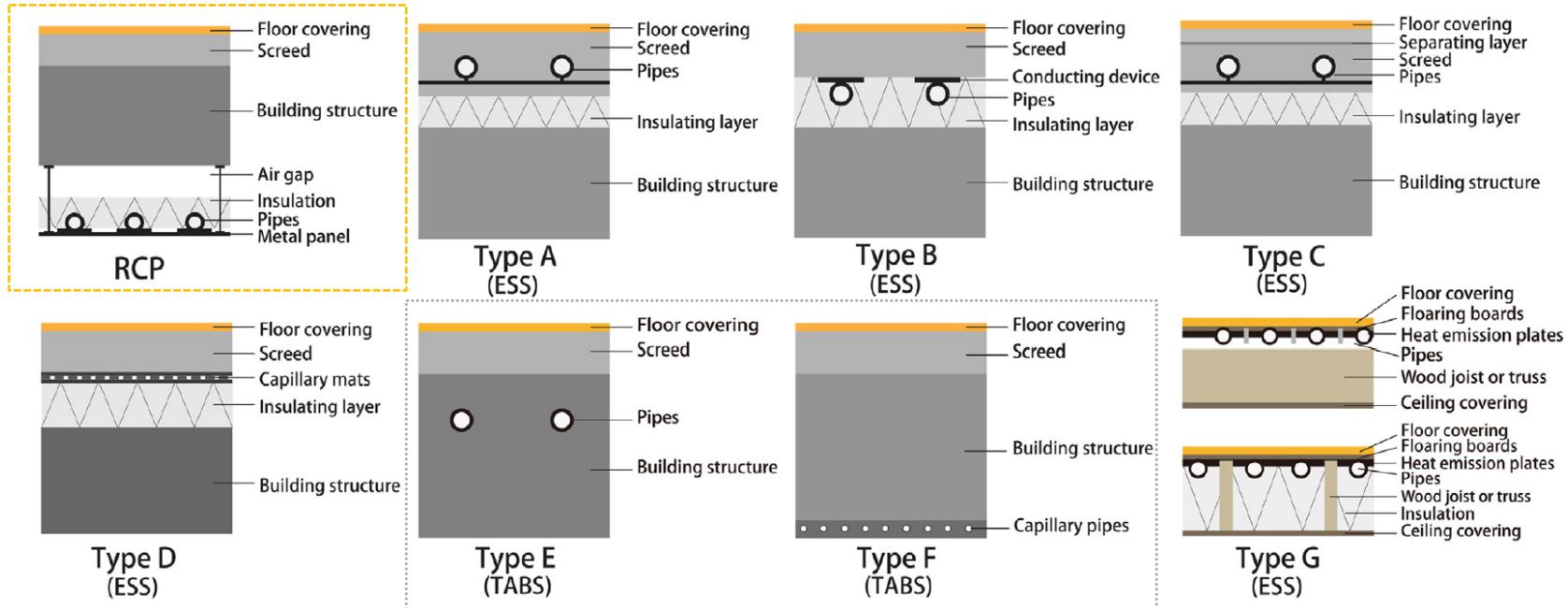
# Radiant Systems

- A system where typically **water** is used as **the heat carrier** (hydronic system) and more than  $\frac{1}{2}$  of the **heat exchange** with **the conditioned space** is by **radiation**.
  - Alternatively, **electric heaters** can also be used as **energy sources**.
- System consists of circuits of **water pipes** **embedded** in floor, wall or ceiling construction.
- Additional **ventilation system** is necessary *to address the latent loads* and to provide the **ventilation rates required** for **indoor air quality**.
- Radiant systems enable **lower air flow rates** than all-air convective systems.



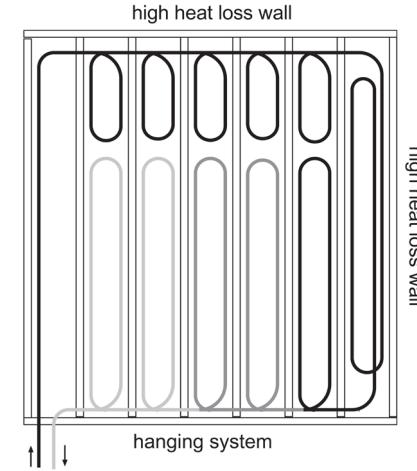
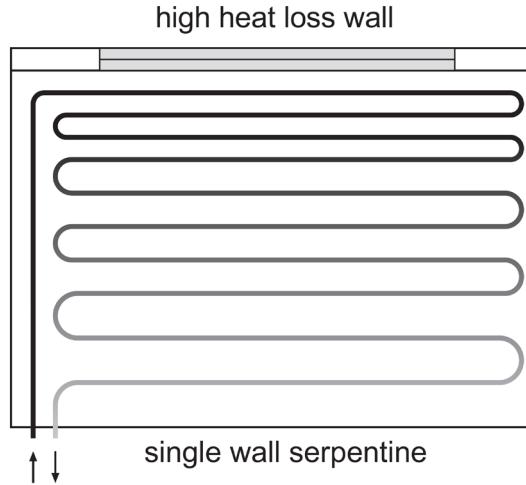
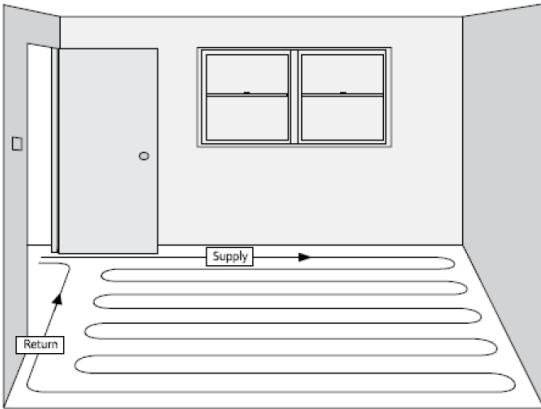
# Hydronic Radiant Systems: Typology

- Three main categories of hydronic systems:
  - **radiant ceiling panels (RCP)**,
  - **embedded surface systems (ESS)**
  - **thermally activated building systems (TABS)**



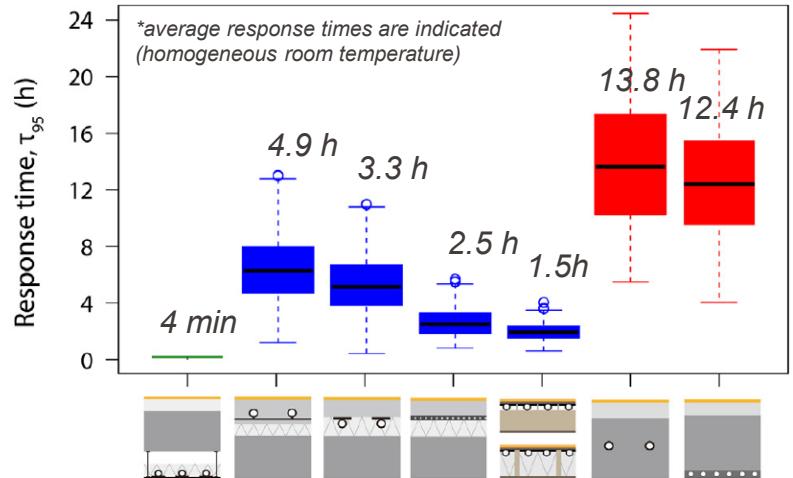
# Radiant Systems: Active Surface Area

- **Active surface area** - the surface area conditioned by the *embedded radiant system*
- The **layout of the piping** should consider *variable* heating and cooling demand, i.e., supply the hottest water to the zones with the highest heat losses
- **Water temperature** at the **inlet** corresponds to maximum circulating water temperature required to provide the maximum loads.
- **Piping layouts for floor systems** a single/double/triple-wall **serpentine**, a **counter flow**, and a **reverse-return**



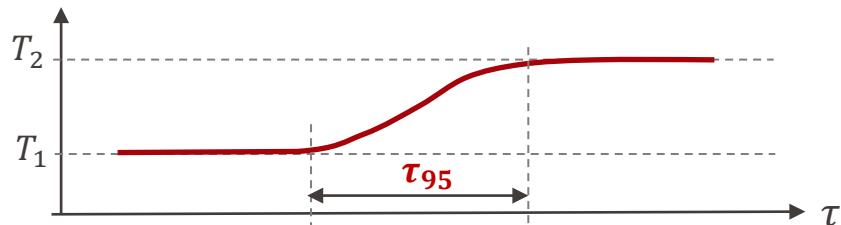
# Hydronic Radiant Systems: Response Time

- **Response Time** (a simple definition) – the time for the system to change from one *stable* condition to another
- **Response Time ( $\tau_{95}$ )** - the time it takes for the surface temperature of a radiant system to reach 95% of the **difference between its final and initial values** when a step change in control of the system is applied as input.
- **Determining parameters:**
  - **Geometric parameters**  
(pipe spacing; pipe diameter, concrete thickness, pipe-embedded depth)
  - **Thermal properties**  
(concrete type, floor covering material)
  - **Boundary conditions**  
(operative temperature, water temperature)



Geometry classification	RCP	Type A	Type B	Type D	Type G	Type E	Type F
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Response time classification	Quick response	Medium response	Slow response
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# Thermally Activated Building Systems (TABS)

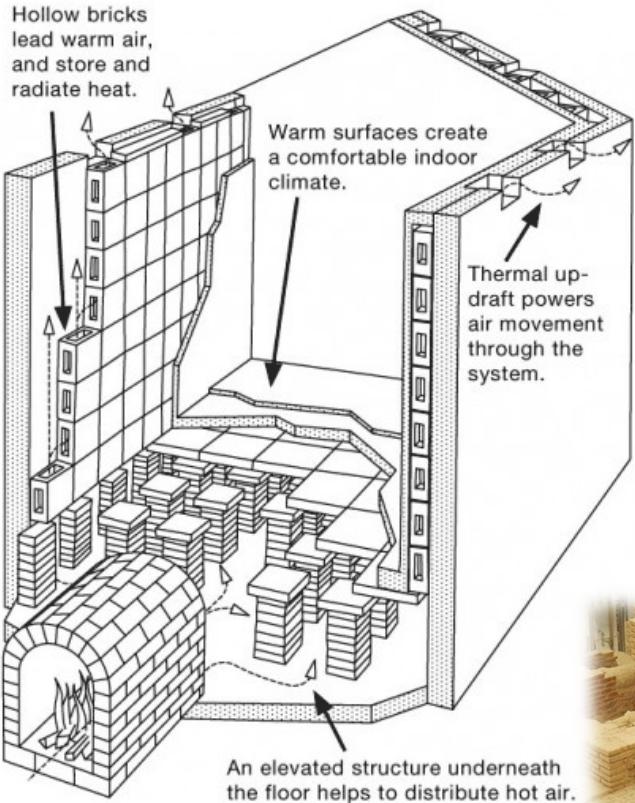


VS

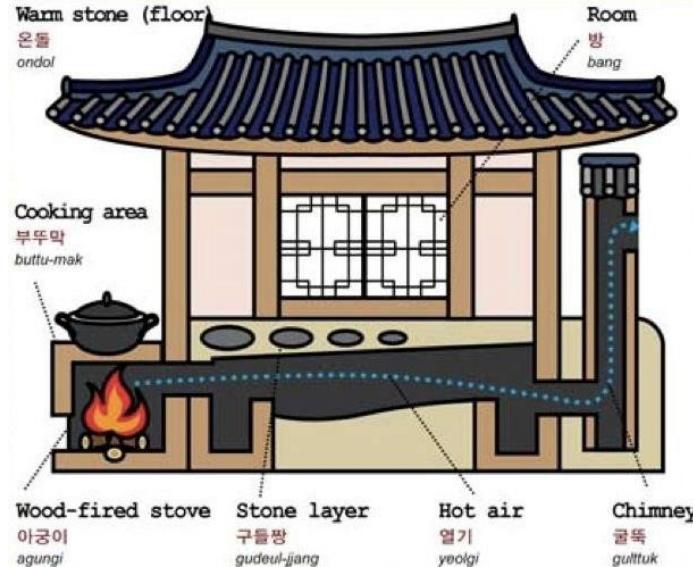


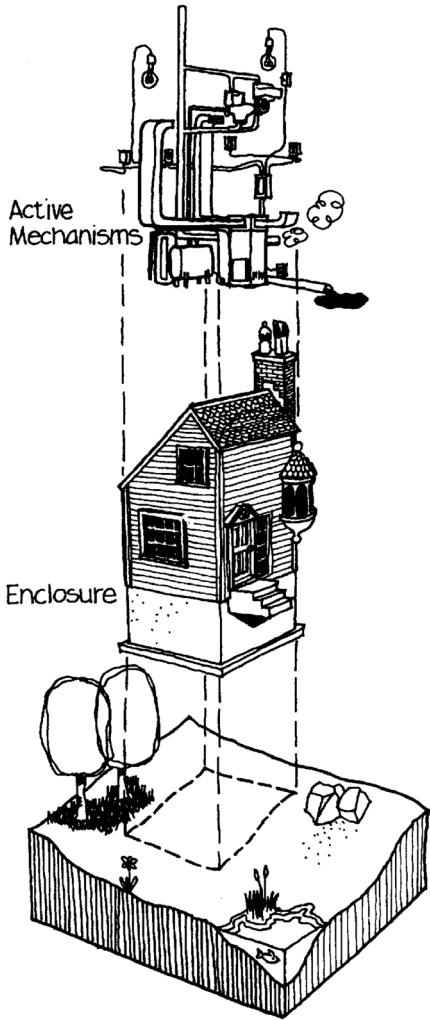
# Radiant Floor Heating: Old New?

## Roman Hypocaust heating (350 BC):



## Traditional Korean heating (Ondol, 5000 BC):

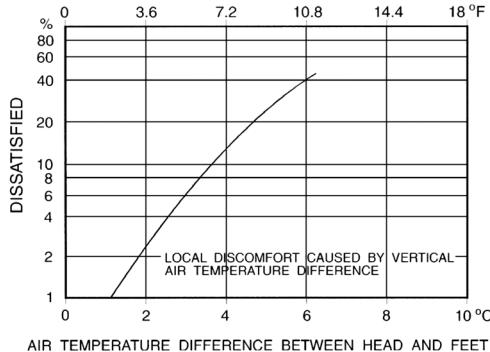
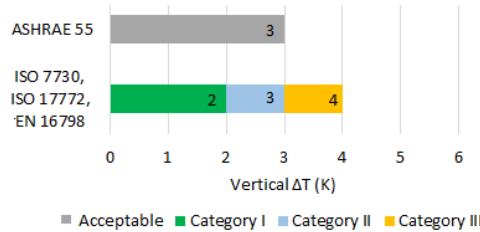




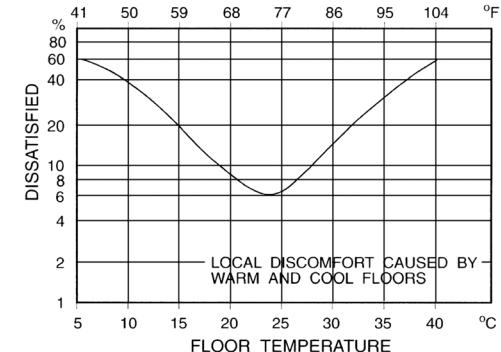
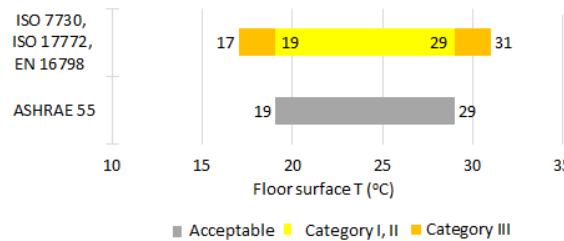
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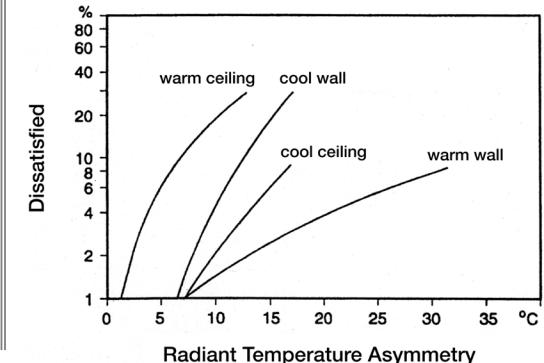
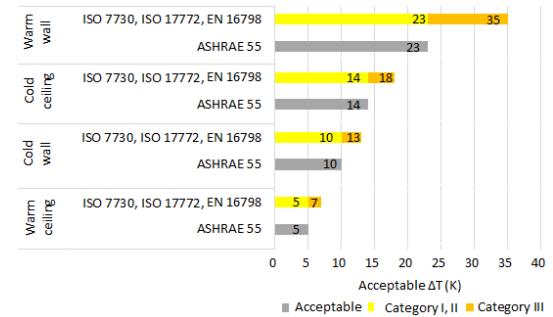
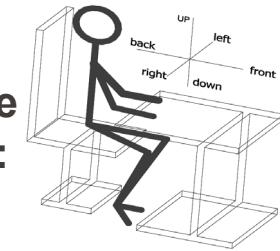
## Vertical Air Temperature Difference:



## Floor Surface Temperature:



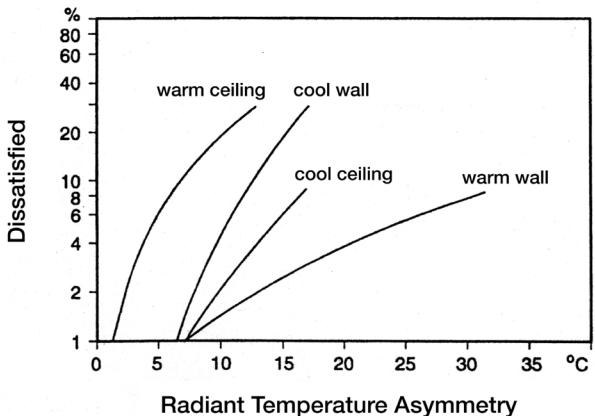
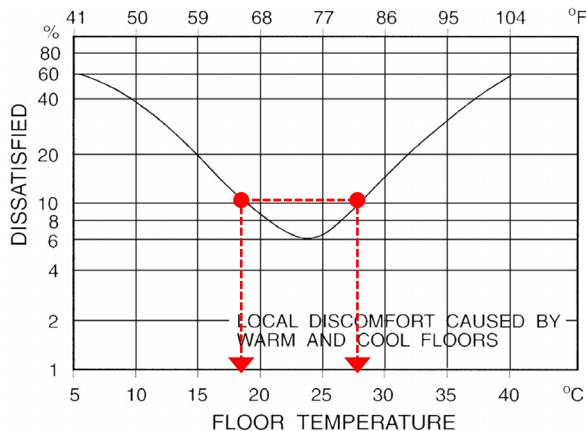
## Radiant Temperature Asymmetry:



# Radiant Systems: Surface Temperature Limits

- The maximum surface temperature depends on the criteria for **radiant asymmetry** and **direct contact with the surface**
- Temperature limits per ISO 7730 for surfaces (floor: occupants with normal shoes - Europe, America):  
**Floor: +29°C / Ceiling: +27°C / Walls: +40°C**
- Acceptable range for **floor surface** should be adjusted for a certain lifestyle (i.e., in Japan and Korea, occupants spend lots of time sitting on the floor):

ASHRAE Fundamentals handbook, 2009	According to the material of the floor	Textiles (rugs): 21≈28°C Pine floor: 22,5≈28°C Oak floor: 24,5≈28°C Hard linoleum: 24≈28°C Concrete: 26≈28,5°C	In America and Europe
Song, GS et al., 2001	According to the material of the floor	Clay: 24,9≈31,5°C Pine: 18,1≈29,0°C Urethane: 12,7≈23,2°C Veneer: 24,7≈31,0°C	In Korea
Ling Zhang et al.		Allowable range of floor surface temperature: 25≈31°C Comfortable range of floor surface temperature: 26≈30°C	In Japan



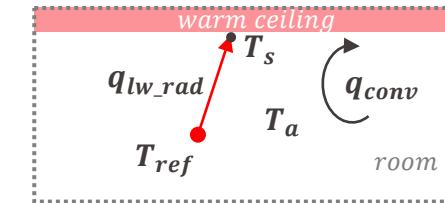
# Embedded Radiant Systems: Rated Heat Flux

- Surface convective heat transfer:
- Longwave radiation heat transfer:
- Total surface heat flux\*:  
(heat flow density,  $\text{W/m}^2$ )

$$q''_{conv} = h_c \times (T_a - T_s)$$

$$q''_{lw\_surf} = h_{rad} \cdot (T_s - T_{ref})$$

$$q = h_t \cdot |T_s - T_{ref}|$$



$T_s = T_{m,s}$  mean surface temperature

$T_{ref} = T_{op}$  operative temperature (per ISO 18555)

Combined convection and (longwave) radiation heat transfer coefficient  $h_t$ :

Heating:		Cooling	
Floor heating (FH)	11 $\text{W/m}^2\text{K}$	Floor cooling (FC)	7 $\text{W/m}^2\text{K}$
Wall heating (WH)	8 $\text{W/m}^2\text{K}$	Wall cooling (WC)	8 $\text{W/m}^2\text{K}$
Ceiling heating (CH)	6 $\text{W/m}^2\text{K}$	Ceiling cooling (CC)	11 $\text{W/m}^2\text{K}$

Radiant (longwave) heat transfer coefficient  $h_{rad} = 5.5 \text{ W/m}^2\text{K}$   
(less than 4% error for surface temperatures in the range of 15-30°C)

- Heat flow density ( $\text{W/m}^2$ ): at steady-state

- **floor heating / ceiling cooling:**  $q = 11 \cdot |T_{m,s} - T_{op}|$
- **wall heating / wall cooling:**  $q = 8 \cdot |T_{m,s} - T_{op}|$
- **ceiling heating:**  $q = 6 \cdot |T_{m,s} - T_{op}|$
- **floor cooling:**  $q = 7 \cdot |T_{m,s} - T_{op}|$

\* Shortwave radiation heat transfer is not considered in the standard approach of defining total heat flow density which might become problematic for floor cooling with direct sunlight

# What is the **comfort-related limiting heat flux** for **FLOOR heating** in the case of **indoor operative temperature 20°C**?

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- A. 80 W/m<sup>2</sup>
- B. 90 W/m<sup>2</sup>
- C. 100 W/m<sup>2</sup>
- D. None above

# What is the comfort-related limiting heat flux for **CEILING** heating in the case of indoor operative temperature 20°C?

- A. 32 W/m<sup>2</sup>
- B. 42 W/m<sup>2</sup>
- C. 52 W/m<sup>2</sup>
- D. None above

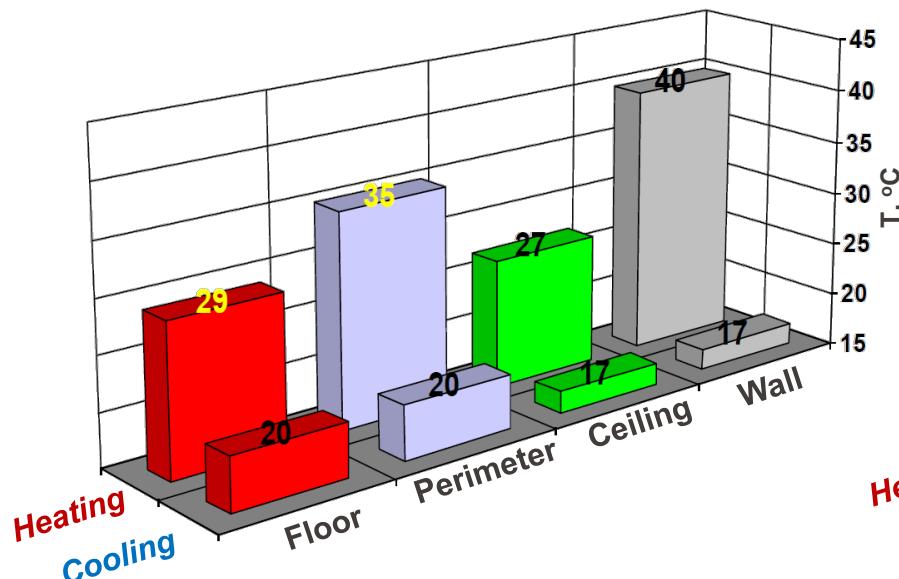
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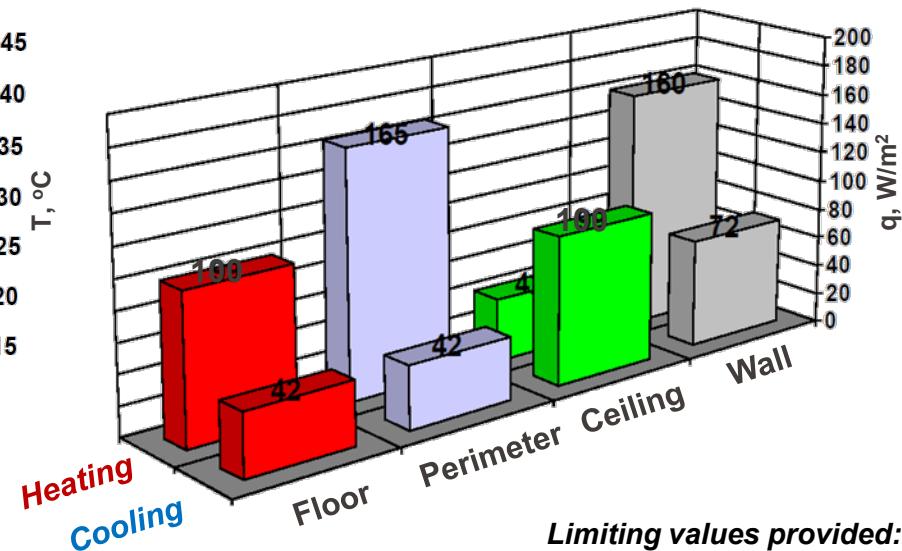
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# Radiant Systems: Maximum Heat Output

- Maximum heating and cooling capacity depends on the position of the radiant surface
- The heating/cooling capacity is limited by relatively small convective heat transfer coefficient between the surface and air, risk of condensation and concerns about surface temperature, radiant asymmetry, vertical air stratification and draft from comfort perspective



Source: Olesen (2018), Radiant heating/cooling dimensioning



**Limiting values provided:**

- for heating:  $T_{op} = 20^\circ\text{C}$
- for cooling:  $T_{op} = 26^\circ\text{C}$

(for  $V_{air} < 0.2 \text{ m/s}$ )

- In heat exchangers, **the heat transfer** between **the hot stream** (water) and **the cold stream** (room air) occurs over **a finite area  $A_s$**  of the heat exchange.
- To determine the heat transfer  $Q$  [W] in heat exchangers, **LMTD method** can be used
  - LMTD** [K] - log-mean temperature difference
  - $U$**  [ $W/m^2K$ ] – overall heat transfer coefficient

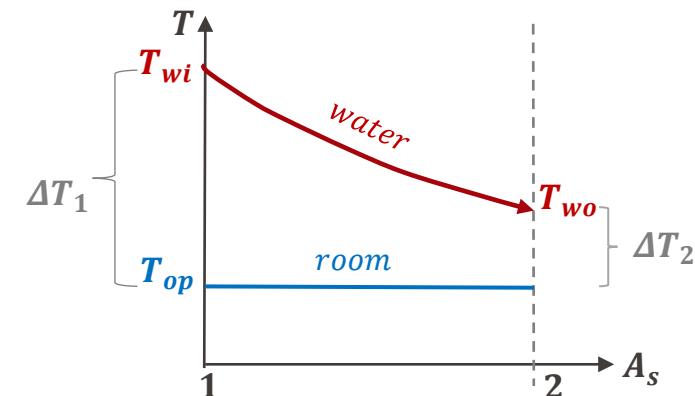
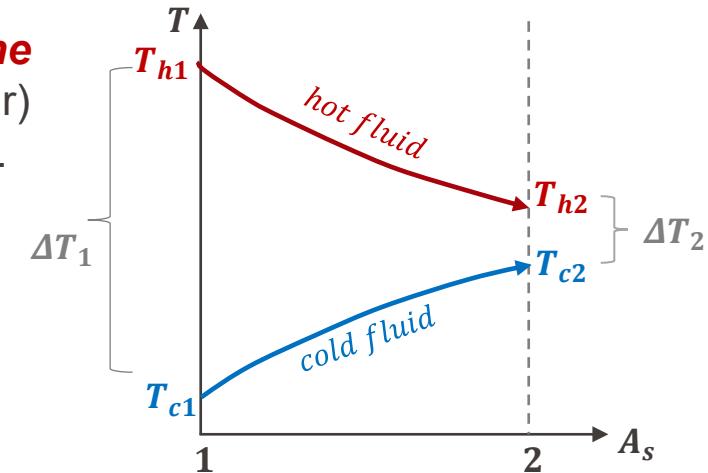
$$Q = U \cdot A_s \cdot \Delta T_{lm}$$

$$\Delta T_{lm} = \frac{\Delta T_1 - \Delta T_2}{\ln[\Delta T_1 / \Delta T_2]}$$

- LMTD** considering constant operative temperature  $T_{op}$  to be maintained indoors:

$$\Delta T_1 = T_{wi} - T_{op}, \quad \Delta T_2 = T_{wo} - T_{op}$$

$$\Delta T_{lm} = \frac{(T_{wi} - T_{wo})}{\ln[(T_{wi} - T_{op}) / (T_{wo} - T_{op})]}$$



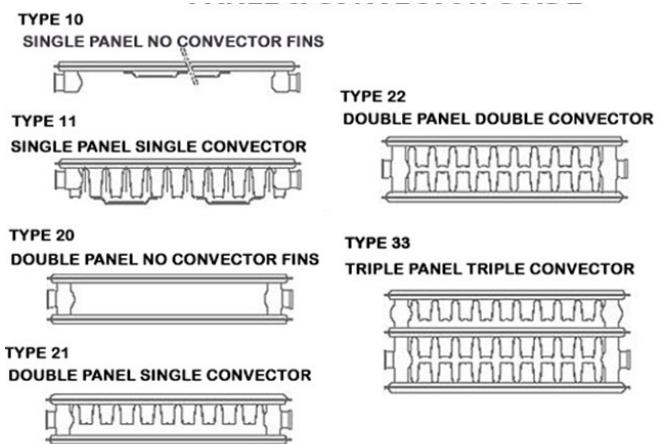
# Radiators/Convector: Selection

1. Determine the room peak heating demand  $Q_{demand}$
2. Measure the room size and space available
3. Choose type of the radiator (i.e., type 11, 22, 33, etc.)
4. Choose required device from a manufacturer's catalogues and determine  $Q_{fabricant}$  close to  $Q_{demand}$
5. Determine exponent  $n$  value indicated in the catalogue
6. Typical water temperature drop ( $T_{wi} - T_{wo}$ ) in radiators is **limited to 10 K**
7. Determine water temperature using the following formulation considering (7):

$$Q_{demand} = Q_{fabricant} * \left( \frac{\Delta T_{actual}}{\Delta T_{standard}} \right)^n$$

where  $\Delta T_{actual} = \frac{(T_{wi} + T_{wo})}{2} - T_{room}$

$\Delta T_{standard} = 50K$  (see the catalogue)

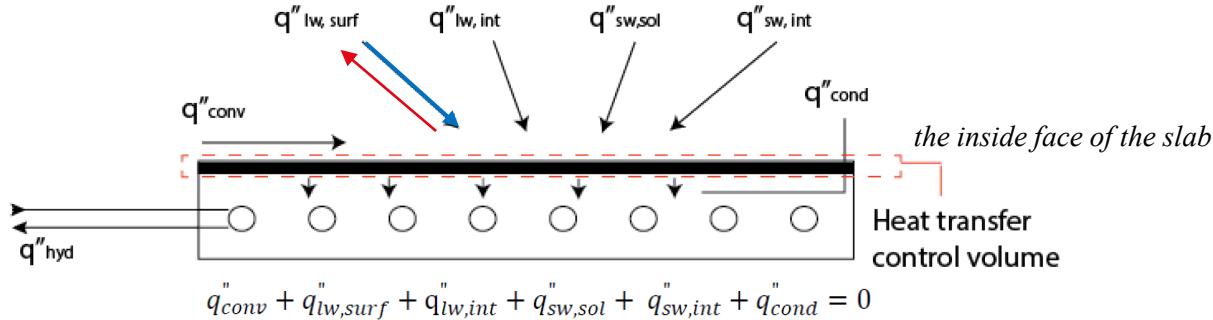


		type 10							
		hauteur							
longueur	watt	300	400	450	500	600	750	900	
450	$\Delta T 50$	145	186	206	225	263	318	370	
600	$\Delta T 50$	193	248	275	301	351	424	493	
750	$\Delta T 50$	242	310	344	376	439	530	617	
900	$\Delta T 50$	290	372	412	451	527	635	740	
1050	$\Delta T 50$	338	434	481	526	614	741	863	
1200	$\Delta T 50$	386	496	550	601	702	847	986	
1350	$\Delta T 50$	435	558	618	676	790	953	1110	
1500	$\Delta T 50$	483	620	687	752	878	1059	1233	
1650	$\Delta T 50$	531	681	756	827	965	1165	1356	
1800	$\Delta T 50$	580	743	824	902	1053	1271	1480	
EN 442 - 75/65/20°C		322	413	458	501	585	706	822	
EN 442 - 90/70/20°C		411	526	584	638	745	899	1046	
valeur n		1,3325	1,3307	1,3297	1,3288	1,3270	1,3242	1,3215	

Source: <https://www.radson.com/docs/Radson-Fiche-technique-CLD-FR.pdf>

Source: <http://cruzoe.free.fr/enr/donn%20es%20diverses/Les%20radiateurs%20Calculs.pdf>

- **Two heat transfer (HT) processes** involved:
  - HT *between the surface of the radiant layer and the space it is conditioning*
  - The HT *between the radiant layer and the water loop*



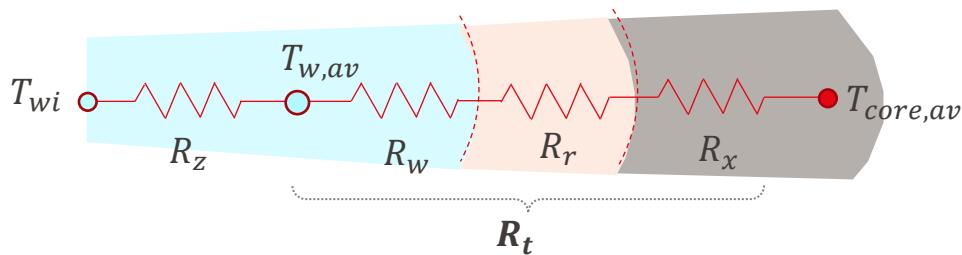
The amount of **heat supplied** by an activated **heating surface** is a **combination** of *convection* and *radiation*:

$$q''_{surf} = -q''_{cond} = q''_{conv} + q''_{lw,surf} + q''_{lw,int} + q''_{sw,sol} + q''_{sw,int} = q''_{conv} + q''_{rad,surf}$$

$$q''_{hyd} = (\dot{m}c_p)_{water}(T_{wi} - T_{wo})$$

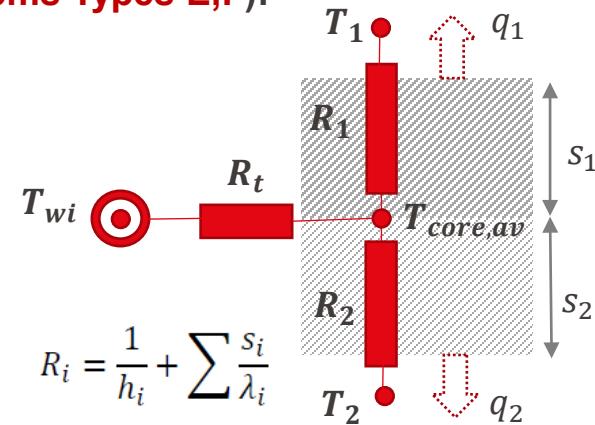
$$\begin{aligned} \dot{m} &= \text{Mass flow rate of water, kg/s;} \\ c_p &= \text{Specific heat of water J/kg} \cdot \text{K;} \\ T_{wi}, T_{wo} &= \text{Supply and return water temperature respectively, } ^\circ\text{C.} \end{aligned}$$

- Conduction heat transfer is *the major* heat transfer mechanism *between the surfaces* and *the hydronic loop* once *heat has been absorbed* by the radiant surfaces
- Thermal resistance network in the slab and between the slab and water loop is used to solve the conduction problem to determine the cooling/heating capacity for **Type E** and **F** systems
- Heating capacity estimation using resistance method (**systems Types E,F**):



- $R_t$  - total resistance between the heat source and the conducting layer
- $R_z$  - resistance between the supply water at temperature  $T_{wi}$  and the average water at temperature  $T_{w,av}$
- $R_w$  - resistance between water at average temperature  $T_{w,av}$  and internal wall surface of the pipe ( $1/h_w$ )
- $R_r$  - resistance between water and the outside pipe wall
- $R_x$  - resistance between the pipe outside wall temp. and the conductive layer (a fictive core) at average temp. of  $T_{core,av}$
- $R_i$  - thermal resistance *in the heat-conducting layer* (from the heat-conducting plate to the room above "1" or below "2")

Source: ISO 11855-2:2012



$$q'' = K_H \cdot \Delta T_h$$

$$K_H = 1/(R_t + R_i)$$

- **Universal power law** (for embedded systems **Type A, B, C, D**):

- **Heat flux at a surface:**  $q'' = K_H \cdot \Delta T_h^n$  , where  $1 < n < 1.05$

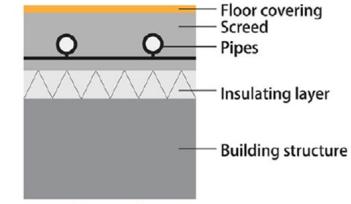
- **Mean temperature difference** between heat carrier (water) and the space:

$$\Delta T_h = \frac{(T_{wi} - T_{wo})}{\ln \left[ \left( T_{wi} - T_{op} \right) / \left( T_{wo} - T_{op} \right) \right]}$$

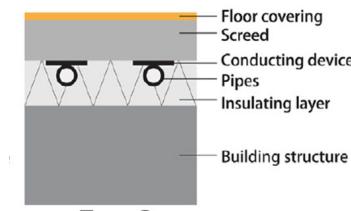
- **Lumped thermal resistance:**  $K_H = B \cdot \prod (a_i^{m_i})$

system dependent coefficient,  $W/(m^2K)$

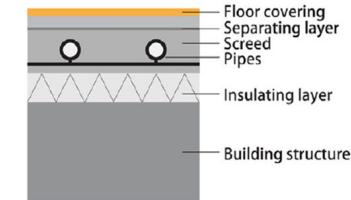
a power product linking parameters of the structure



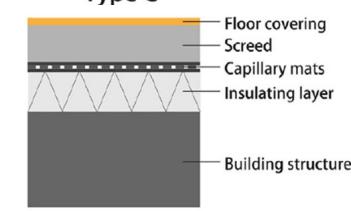
Type A



Type B

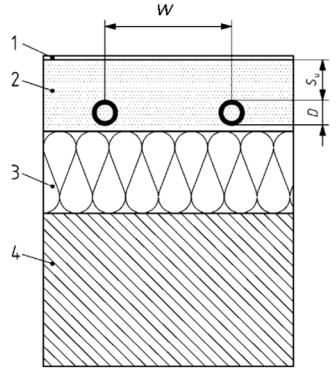


Type C



Type D  
(ESS)

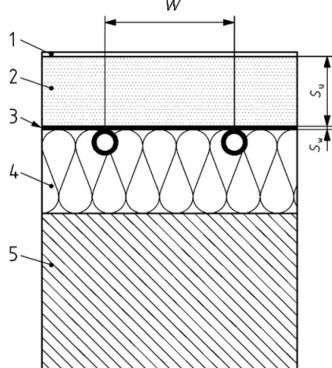
## Systems Types A, C:



$$q = B \cdot a_B \cdot a_W^{m_w} \cdot a_U^{m_u} \cdot a_D^{m_D} \cdot \Delta T_h$$

$$B=6.7 \text{ W}/(\text{m}^2\text{K})$$

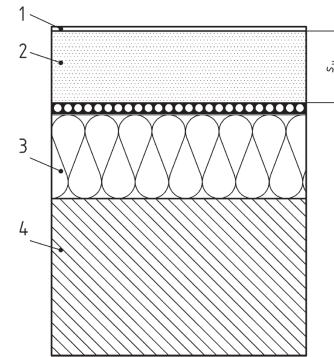
## System Type B:



$$q = B \cdot a_B \cdot a_W^{m_w} \cdot a_U \cdot a_{WL} \cdot a_K \cdot \Delta T_h$$

$$B=6.5 \text{ W}/(\text{m}^2\text{K})$$

## System Type D:



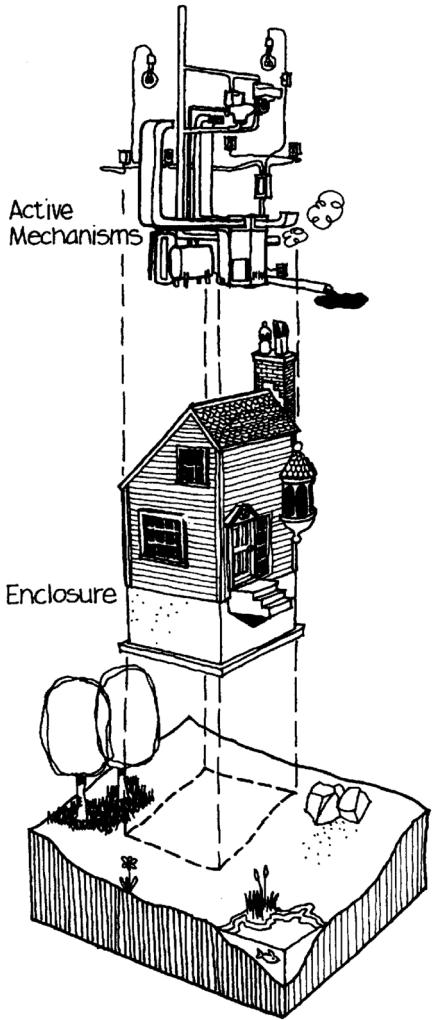
$$q = B \cdot a_B \cdot a_W^{m_w} \cdot a_U \cdot \Delta T_h$$

$$B=6.5 \text{ W}/(\text{m}^2\text{K})$$

- $a_B$  - surface covering factor
- $a_W$  - the pipe spacing factor,  $f(R_{\lambda,B})$
- $a_U$  - the screed covering factor,  $f(W, R_{\lambda,B})$
- $a_D$  - the pipe external diameter factor,  $f(W, R_{\lambda,B})$
- $a_B$  - heat conduction device factor,  $f(K_{WL}, W, D)$
- $a_K$  - correction factor for the contact,  $f(W)$

Values are  
tabulated in  
ISO 11855

- Factor considering spacing of pipes:  
 $m_w = 1 - W/0.075$
- Factor considering covering thickness:  
 $m_u = 100 \cdot (0.045 - s_u)$
- Factor considering diameter of pipes:  
 $m_D = 250 \cdot (D - 0.020)$



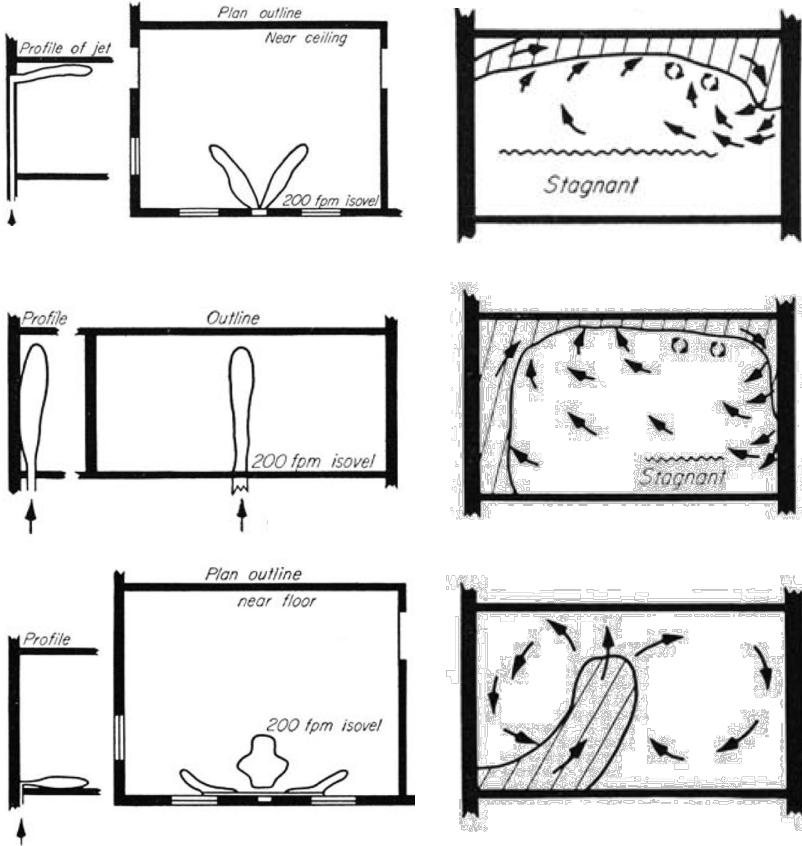
Source: Edward Allen «How Buildings Work» (2005)

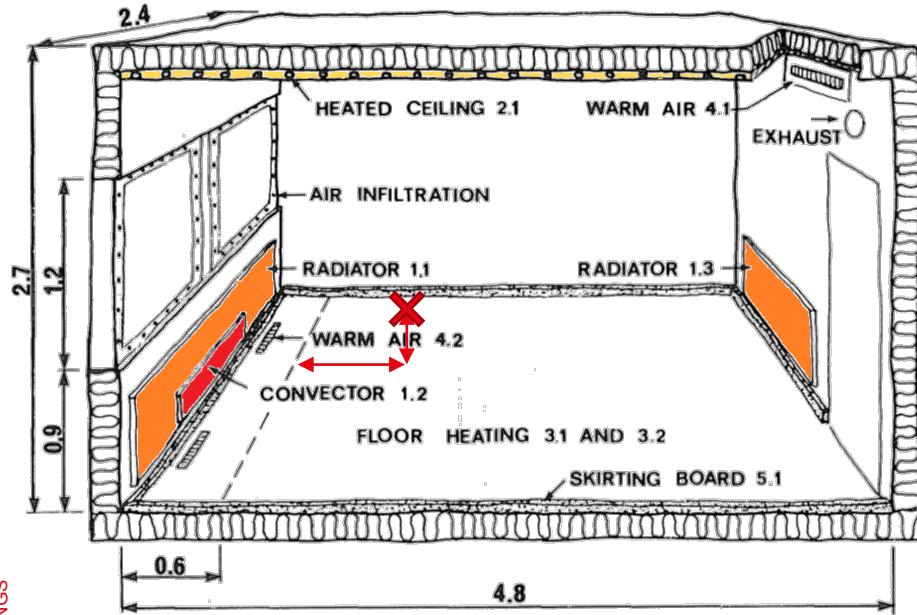
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## Distinct groups of air patterns:

- Air is discharged at the ceiling level
- Air is discharged vertically from floor grill (non-spreading floor outlet)
- Air spread horizontally across the floor (long baseboard units that spread air over a wide floor area)





- Test room:  $4.8 \times 2.4 \times 2.7 \text{ m}^3$
- Outside air temperature simulation:  $-5^\circ\text{C}$  and  $+4^\circ\text{C}$  (only for the front wall with windows)
- Multiple space heating approaches **comparison** for **PMV=0** condition *at the reference point (1 m away from window at the height of 0.6 m)*

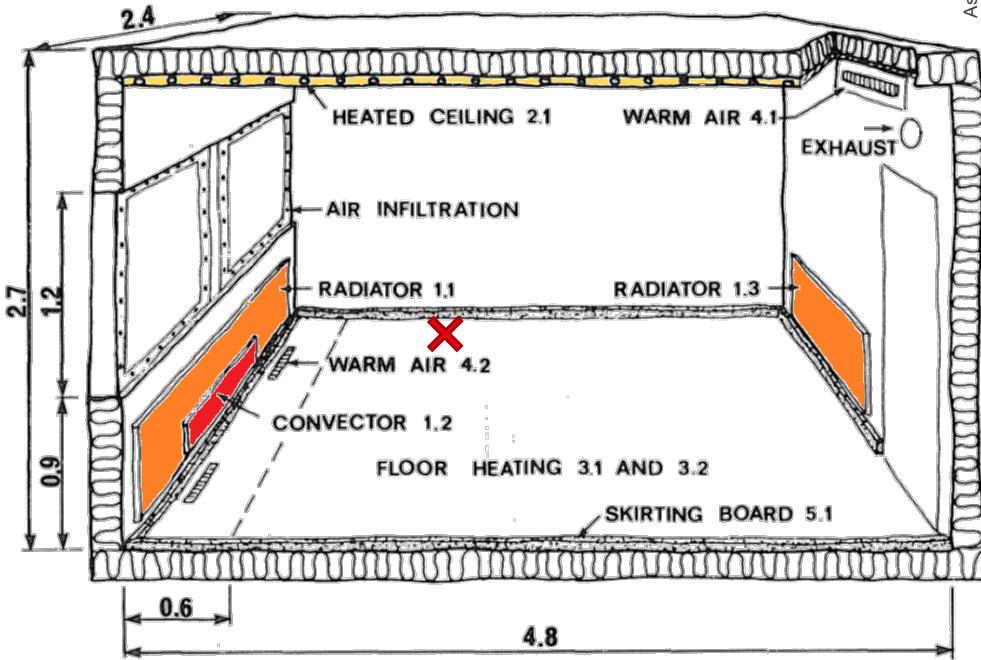
No	Emission	Description	Heat carrier	$T_{\text{supply}} (\text{°C})$
1.1	Radiator	Single panel radiator beneath the window covering most of the lower wall	Warm water	37-48
1.2	Convector	3 panel convectors beneath the window	Warm water	39-53
1.3	Radiator	Single panel radiator at the back wall	Warm water	46-63
2.1	Ceiling	Aluminium plates with water-filled coils, supply along the frontage and return at the back wall	Warm water	34-42
3.1	Floor (uniform)	Electrical heating foil covered by a 2 mm aluminium plate (uniform distribution)	El. Heater	--
3.2	Floor (non-unif)	As 3.1, but the effect on a 0.6 m strip along the frontage was higher ( $T_{\text{surf}}=29^\circ\text{C}$ )	El. heater	--
4.1	Warm air	Outlet in the back wall near the ceiling, 4 ACH, $V=1.2 \text{ m/s}$ .	Warm air	34-43
4.2	Warm air	2 outlets in the floor beneath the window, 4 ACH, $V= 1.2 \text{ m/s}$ .	Warm air	34-43
5.1	Skirting board	Small electrical heated panels along the periphery of the room	El. heater	--

# What type of system would lead to the highest vertical air temperature difference at the reference point (X)?

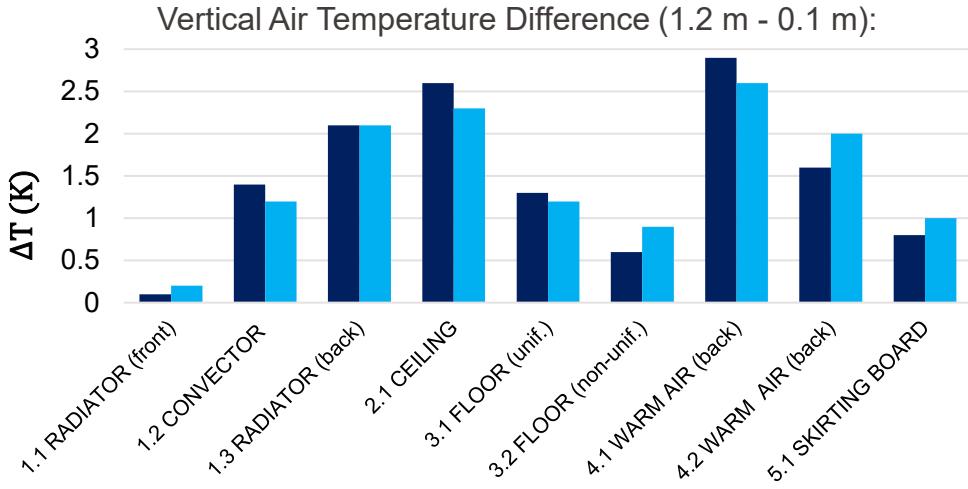
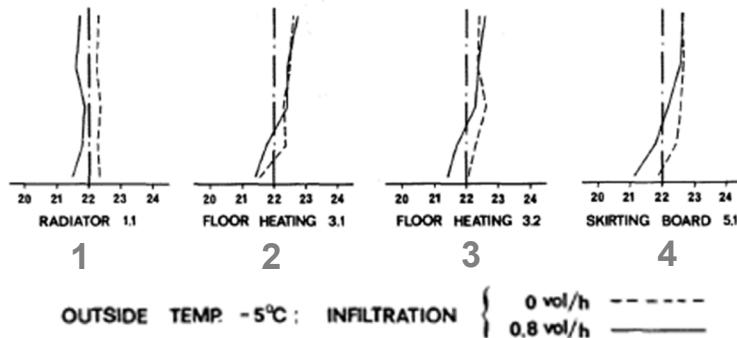
- A. Radiator (1.3)
- B. Warm air (4.1)
- C. Warm air (4.2)
- D. Heated ceiling (2.1)

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- The highest vertical air temperature difference (0.1-1.8m) is for **warm air system (4.1)** with outlet in the back wall near the ceiling, and **a heated ceiling (2.1)**
- Increased air infiltration rate decreased vertical air temperature difference slightly*



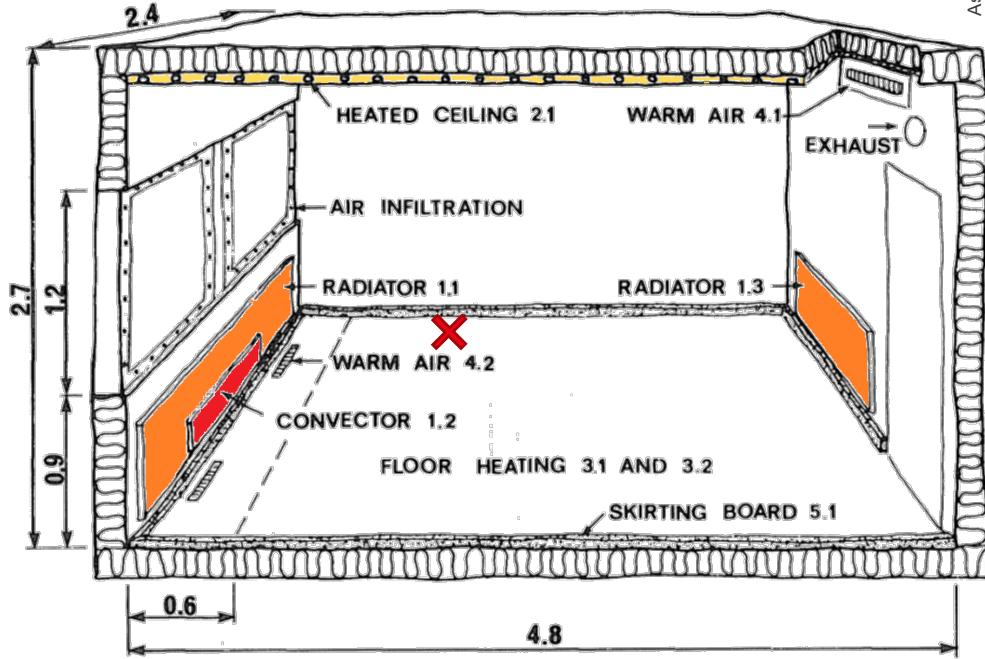
Sources: Olesen B. W. et al. (1978). Thermal comfort in a room heated by different methods

# What type of system would lead to the highest VERTICAL radiant temperature asymmetry at the reference point (X)?

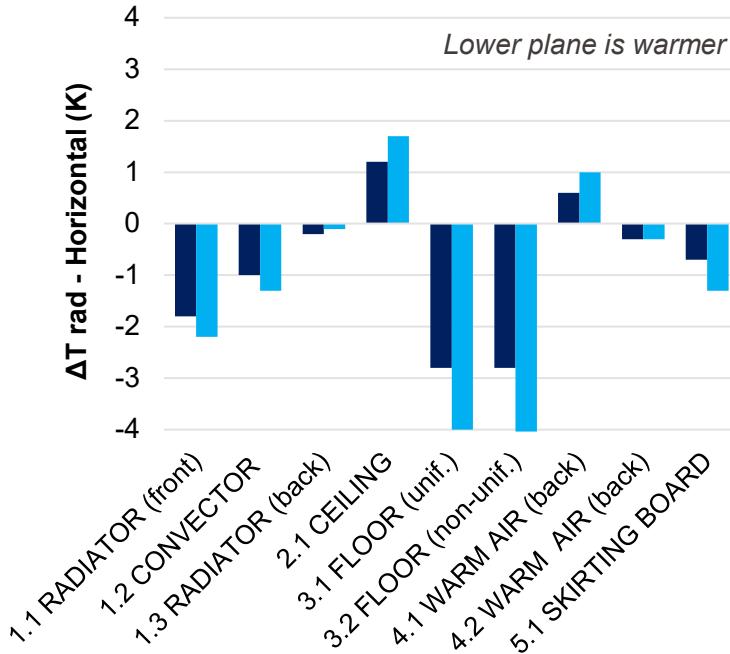
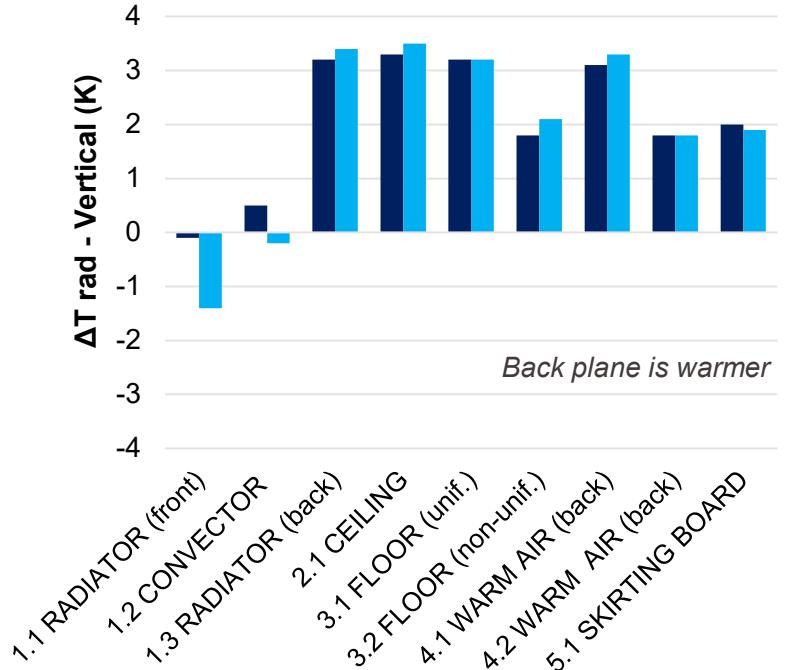
- A. Radiator (1.3)
- B. Warm air (4.1)
- C. Warm air (4.2)
- D. Heated ceiling (2.1)

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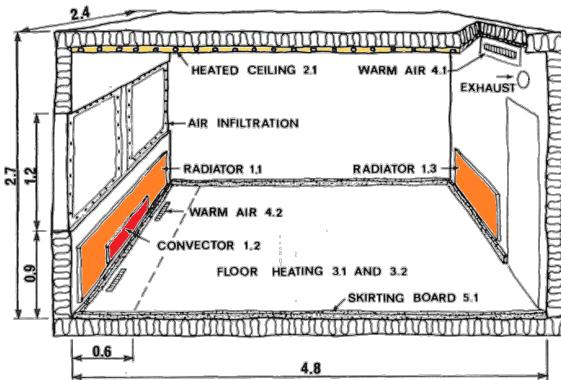
### Radiant Temperature Asymmetry (Vertical & Horizontal Plane):



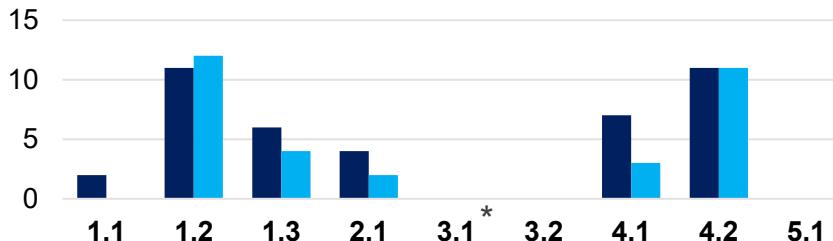
# Heating Systems Comparison: Heat Losses

-5°C, 0 ACH  
-5°C, 0.4 ACH

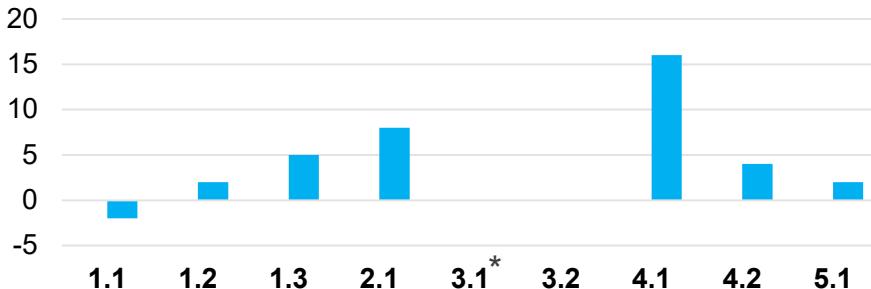
- **Total heat losses:** *the lowest* for the floor heating system (3.1)
- **The heat loss through the window:** *the highest* for **convector** (1.2) and **warm air** (4.2) due to *increased air velocity* and *air temperature* along the window surface (upward natural/forced convection)
- **The heat loss by infiltration:** *the highest* with **warm air** (4.1) system with *air supply from the back*



Heat losses through the window (in %):



Heat losses by infiltration (in %):

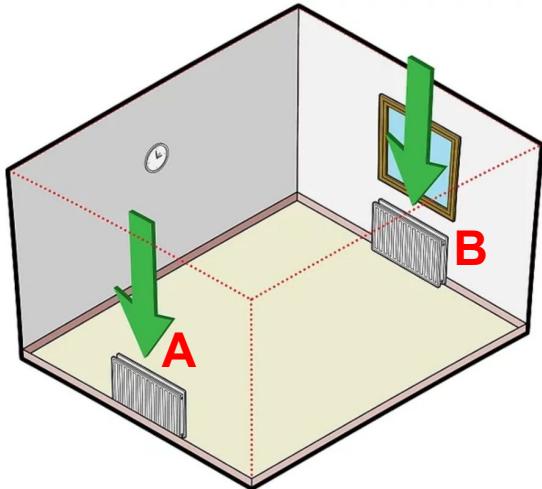


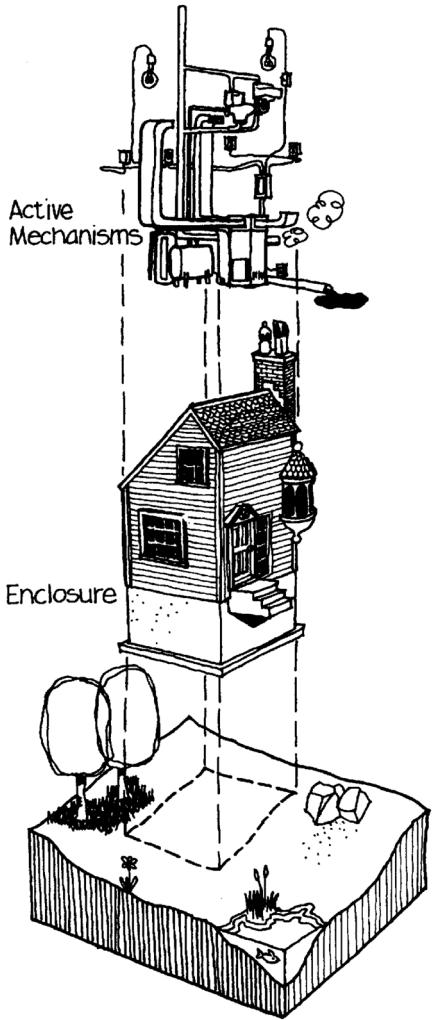
\* Uniform floor heating (3.1) is considered as the baseline

# What is the **optimal location** of the radiator from **comfort** and **energy** perspective?

- A. A
- B. B
- C. Need more information to answer

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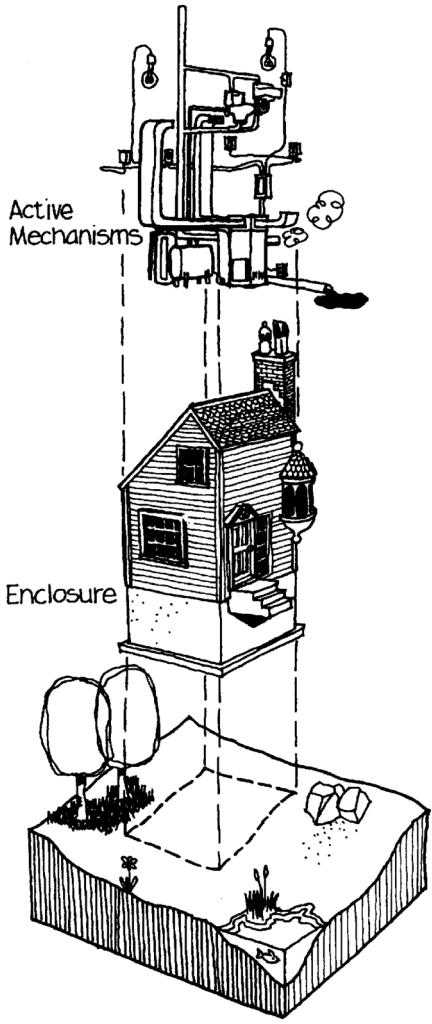
Code	Title
EN 12831-1:2017	Energy performance of buildings - Method for calculation of the design heat load – <b>Part 1: Space heating load</b>
EN 12831-3:2017	Energy performance of buildings - Method for calculation of the design heat load – <b>Part 3: Domestic hot water systems heat load and characterization of needs</b>
EN 15316-2:2017	Energy performance of buildings - Method for calculation of system energy requirements and system efficiencies – <b>Part 2: Space emission systems (heating and cooling)</b>
EN 15316-3:2017	Energy performance of buildings - Method for calculation of system energy requirements and system efficiencies – <b>Part 3: Space distribution systems (DHW, heating and cooling)</b>
EN 15316-4-1:2017	Energy performance of buildings - Method for calculation of system energy requirements and system efficiencies – <b>Part 4-1: Space heating and DHW generation systems, combustion systems (boilers, biomass)</b>

### Swiss Regulations:

SIA 380:2015	Bases pour les calculs énergétiques des bâtiments
SIA 384.201:2017	Performance énergétique des bâtiments - Méthode de calcul de la charge thermique nominale - Partie 1: Charge de chauffage des locaux, module M3-3
SIA 380/1:2016	Besoins de chaleur pour le chauffage

Code	Title
EN 442-1:2014	<b>Radiators and convectors - Part 1: Technical specifications and requirements</b>
EN 442-2:2014	<b>Radiators and convectors - Part 2: Test methods and rating</b>
Code	Title
ISO 18566-1:2017	Building environment design — Design, test methods and control of <b>hydronic radiant heating and cooling panel systems</b> — <b>Part 1: Vocabulary, symbols, technical specifications and requirement</b>
ISO 18566-2:2017	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 2: Determination of heating and cooling capacity of ceiling mounted radiant panels</b>
ISO 18566-3:2017	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 3: Design of ceiling mounted radiant panels</b>
ISO 18566-4:2017	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 4: Control of ceiling mounted radiant heating and cooling panels</b>
ISO 18566-6:2019	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 6: Input parameters for the energy calculation</b>

Code	Title
ISO 11855-1:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 1: Definition, symbols, and comfort criteria</b>
ISO 11855-2:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 2: Determination of the design heating and cooling capacity</b>
ISO 11855-3:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 3: Design and dimensioning</b>
ISO 11855-4:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 4: Dimensioning and calculation of the dynamic heating and cooling capacity of Thermo Active Building Systems (TABS)</b>
ISO 11855-5:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 5: Installation</b>
ISO 11855-6:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 6: Control</b>

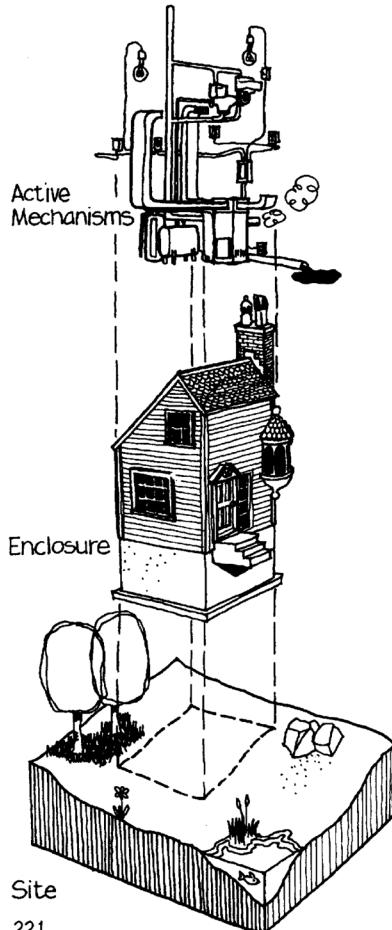


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- **Heating/Cooling Emission Systems Overview**  
Role of emission systems within active heating and cooling systems.
- **Heating Emission Systems Categorization**  
Types of systems: **All-air systems**, **radiators (convectors)**, and **radiant systems**.
  - **All-Air Systems:** Definition, key characteristics, and configuration options.
  - **Radiators/Convectors:** Definition, main features, and common setup types.
  - **Radiant Systems:** Definition, attributes, layout designs, and key considerations.
- **Types of Radiant Systems:** Radiant Ceiling Panels (RCP), Embedded Surface Systems (ESS), and Thermally Activated Building Systems (TABS)
- **Local Thermal Discomfort Overview**  
Impact of radiant asymmetry and surface temperature limits on comfort.
- **Technical Overview/Considerations:** Heat transfer and heat exchanger analysis, rated heat flux, and selection criteria.



Source: Edward Allen «How Buildings Work» (2005)

**Thank you  
for your attention!**

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