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Session ID: **ENG445**



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# **ENG-445**

## **Building Energetics**

### **Heating in Buildings – Emission Systems and Thermal Comfort**

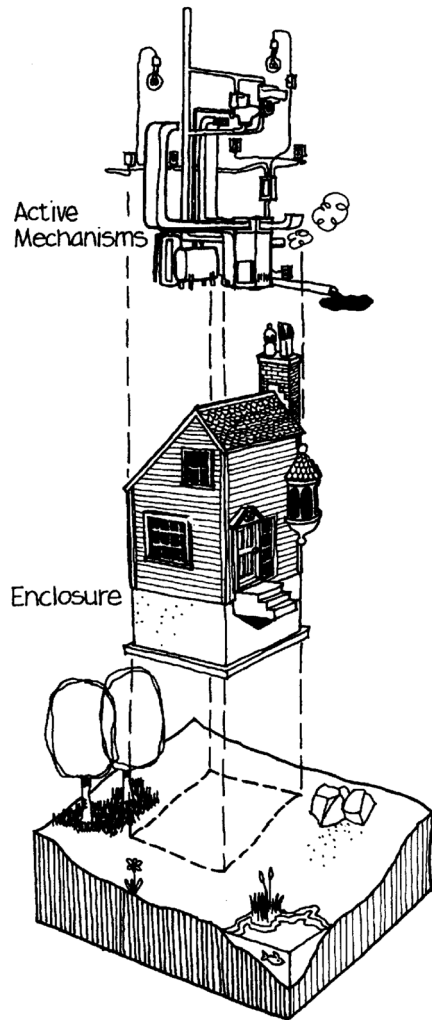
**Dr. Jaafar YOUNES,**  
Assist. Professor  
**Dolaana Khovalyg**

21 November 2024

Week	Date	Topic	Timing	Teacher	Project (AS, MF)
9	07/11	Building envelope, thermal performance of building elements	45' x 2	DK	Tutorial building envelope
		Exercises	45'		
10	14/11	Heating and cooling demand in buildings	45' x 2	DK	Free work
		Exercises	45'		
11	21/11	Thermal systems for heating and their effect of human comfort	45' x 2	JY	Free work
		Exercises	45'		
12	28/11	Thermal systems for cooling and their effect of human comfort	45' x 2	DK	Tutorial heating systems (emission systems)
		Exercises	45'		



JY – Jaafar Younes, a postdoc from the ICE lab

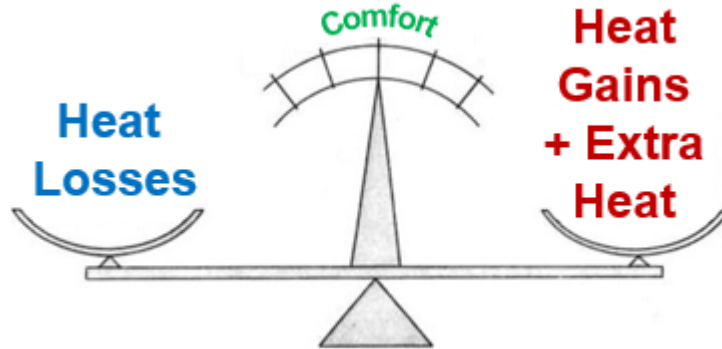
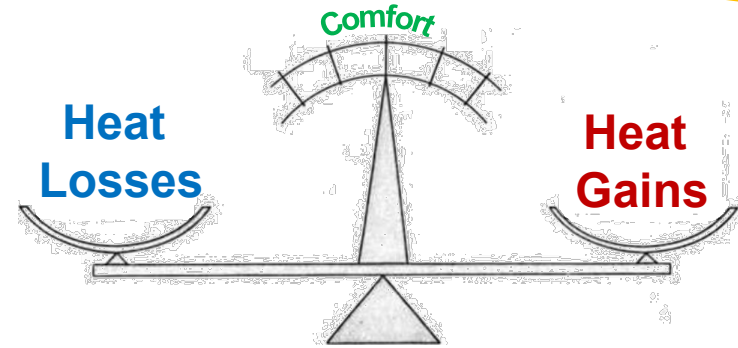


Source: Edward Allen «How Buildings Work» (2005)

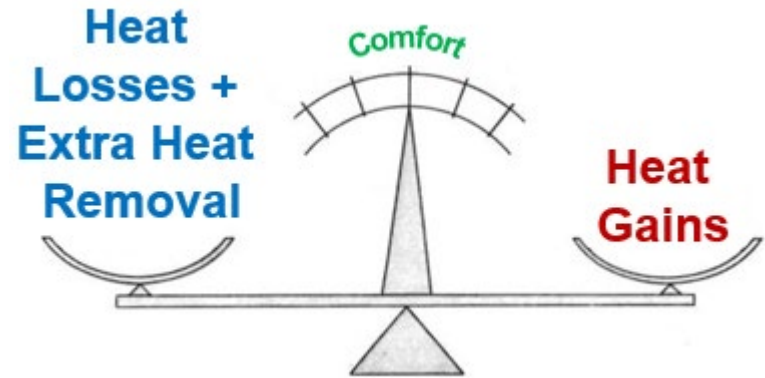
# CONTENT:

- Introduction
- Overview of Emission Systems:
  - Definition
  - All-air systems
  - Radiators (convectors)
  - Radiant systems
- Technical Characteristics
  - Local discomfort limits
  - Convectors vs. Embedded systems
- Thermal Comfort vs. Emission Systems
  - Comparative study overview
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- **Comfortable indoor temperature** is maintained by *balanced* heat losses and heat gains
- **Heating** or **cooling** is needed when they are *imbalanced* and **extra** heat addition or removal is necessary



HEATING



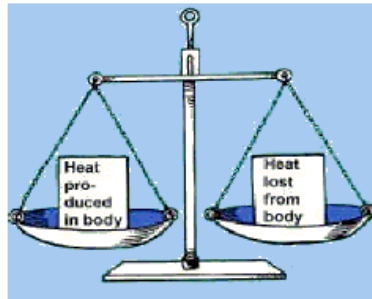
COOLING



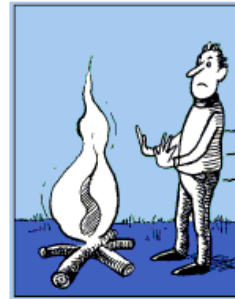
- **Thermal neutrality** for the body as a whole is a necessary, but *not sufficient condition* for thermal comfort.
- **Local thermal discomfort** due to draught, vertical temperature gradient, radiant asymmetry, or warm or cold floors may cause occupants to find **the thermal conditions unacceptable**.

*It is essential to evaluate thermal comfort in 2 steps:*

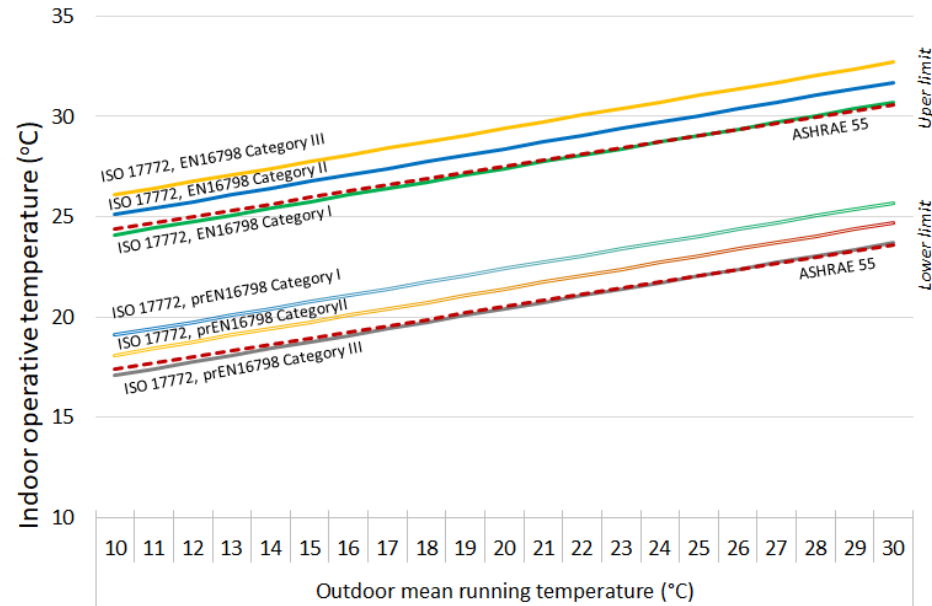
- 1) Define the **acceptable operative temperature**
- 2) Check that **there is no local discomfort**



+



- Considers **thermal comfort** as a **result of adaptation** (physiological, behavioral, psychological)
- A *strong* relationship of the **comfortable temperatures** inside a building with **the mean temperatures prevailing outside the building** for *naturally ventilated* buildings (in 'free-running')



Standard	Categories	$T_{op}$ (°C), upper limit	$T_{op}$ (°C), lower limit	$T_{rm}$ (°C), applicability range
ISO 17772, EN 16798	I	$0.33 \cdot T_{rm} + 20.8$	$0.33 \cdot T_{rm} + 15.8$	10-30
	II	$0.33 \cdot T_{rm} + 21.8$	$0.33 \cdot T_{rm} + 14.8$	10-30
	III	$0.33 \cdot T_{rm} + 22.8$	$0.33 \cdot T_{rm} + 13.8$	10-30
ASHRAE 55	acceptable (80%)	$0.31 \cdot T_{rm} + 21.3$	$0.31 \cdot T_{rm} + 14.3$	10-33.5
	acceptable (90%)	$0.31 \cdot T_{rm} + 21.3$	$0.31 \cdot T_{rm} + 15.3$	

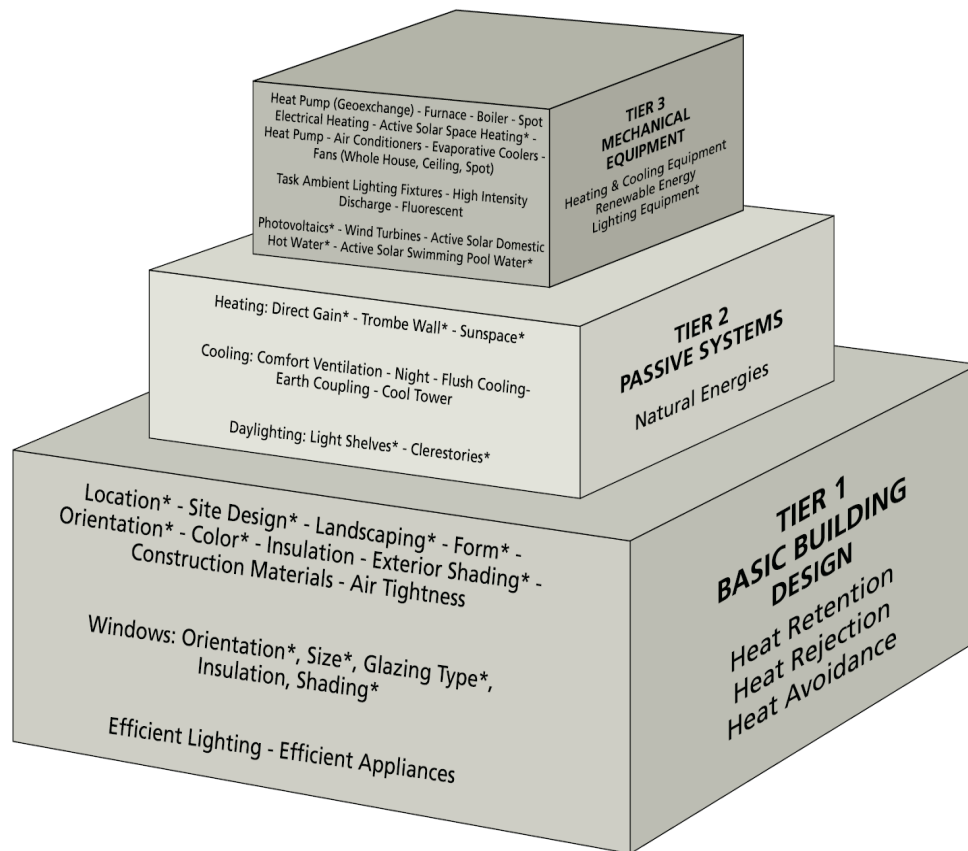
Source: Khovalyg et al. (2019) Energy and Buildings, DOI : 10.1016/j.enbuild.2020.109819.

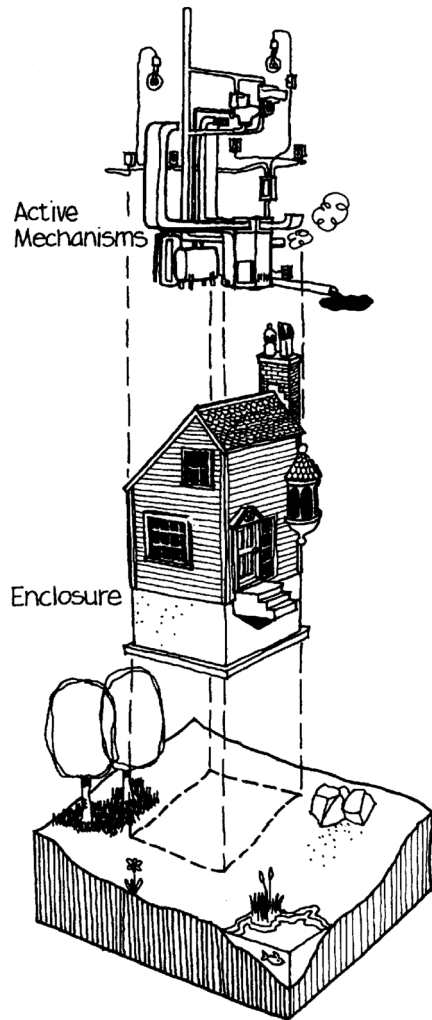
# Three-Tier Design Approach

From Week 10

**Table 1.4A The Three-Tier Design Approach**

	Heating	Cooling
<b>Tier 1</b>	<i>Conservation</i>	<i>Heat avoidance</i>
Basic Building Design	1. Surface-to-volume ratio 2. Insulation 3. Infiltration	1. Shading 2. Exterior colors 3. Insulation 4. Mass
<b>Tier 2</b>	<i>Passive solar</i>	<i>Passive cooling</i>
Natural Energies and Passive Techniques	1. Direct gain 2. Trombe wall 3. Sunspace	1. Evaporative cooling 2. Night-flush cooling 3. Comfort ventilation 4. Cool towers
<b>Tier 3</b>	<i>Heating equipment</i>	<i>Cooling equipment</i>
Mechanical and Electrical Equipment	1. Furnace 2. Boiler 3. Ducts/Pipes 4. Fuels	1. Refrigeration machine 2. Ducts 3. Geo-exchange





Source: Edward Allen «How Buildings Work» (2005)

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## Active (mechanical) Heating/Cooling System

=

**1** Emission system  
(radiators, fan coils, etc.)

+

**2** Distribution system  
(pipe work, ducts, circulation pumps)

+

**3** Storage  
(water tanks, etc.)

+

**4** Generation system  
(heat pump, boiler, etc.)

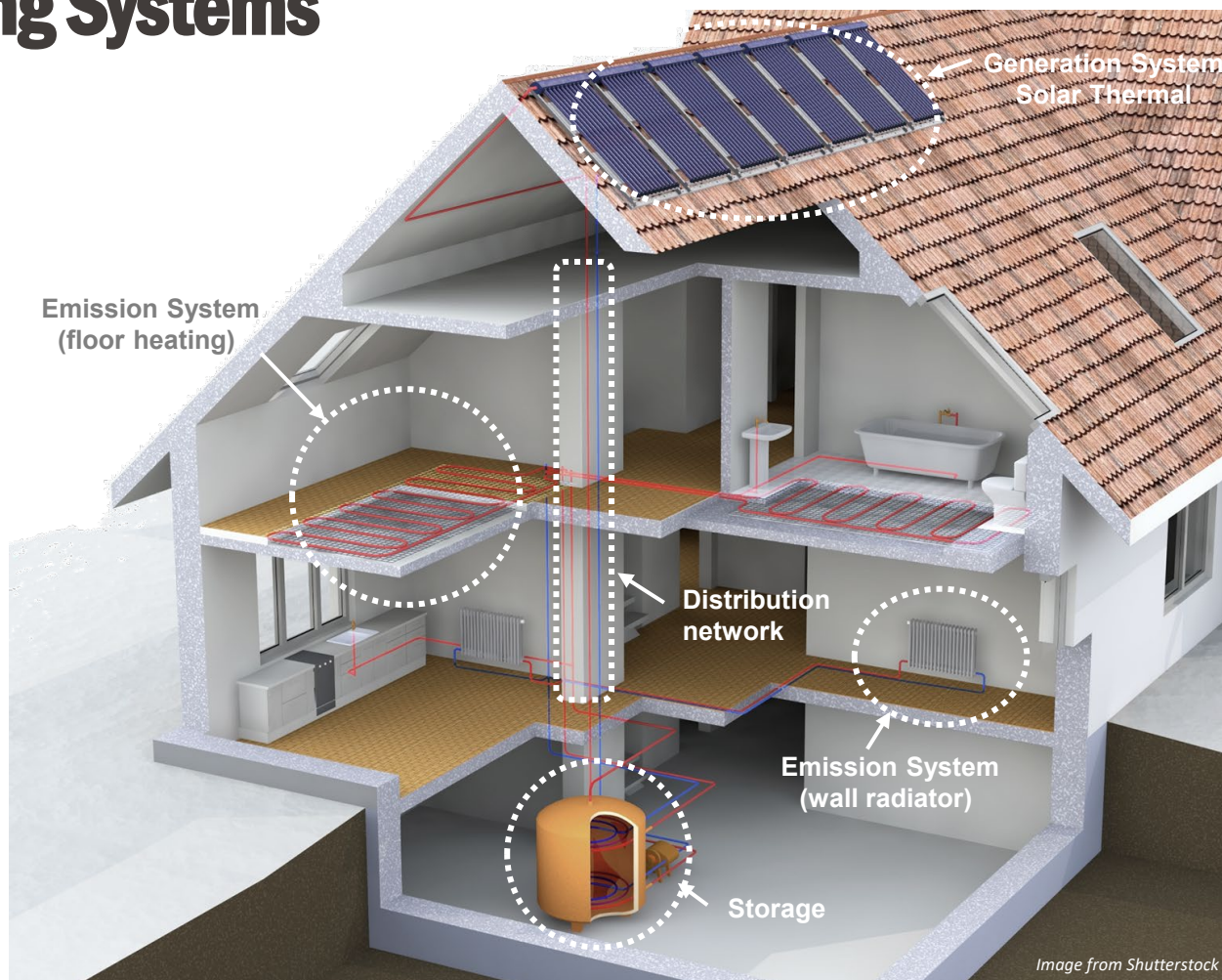
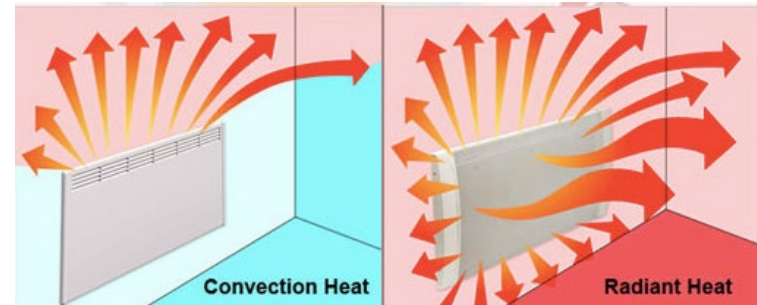
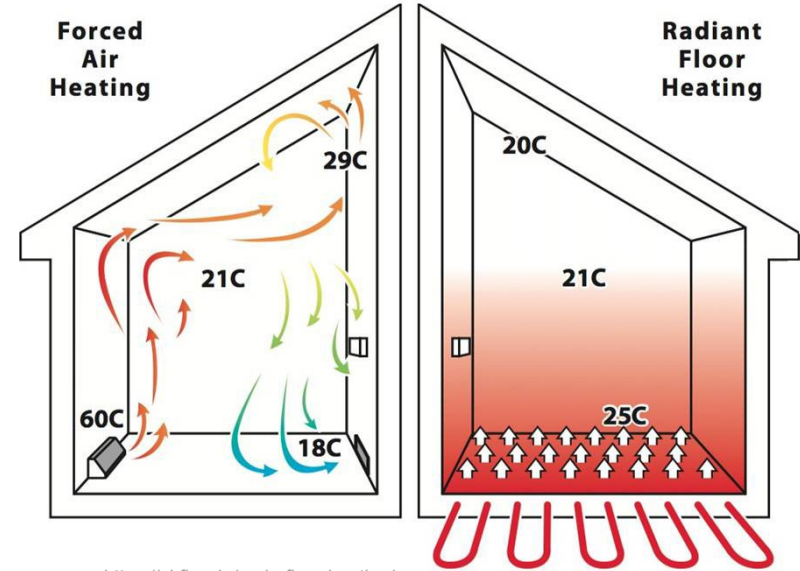


Image from Shutterstock

# Indoor Emission Systems

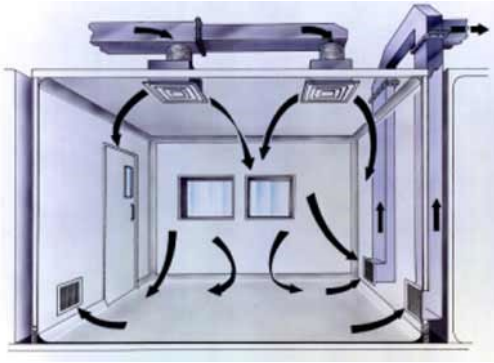
- Multiple ways to name - *indoor emission systems*, *indoor terminal units*, ..
- **Building elements** that use **different heat transfer mechanisms** and **media** to *emit* and *remove heat* and/or *moisture* from indoor spaces
- They differ in their capabilities of *addressing*:
  - **sensible** and **latent loads**
  - **methods** of **heat emission** or **removal**: convection, radiation, combined
  - maximum heating/cooling capacities
  - **medium** of **energy distribution** (i.e., heat carrier) – water, air, electricity
  - **local** or **total volume** conditioning (for convective systems)



## All-Air Systems

**centralized** air conditioning

heat extraction using: **air**



- Air supply through **grills** (no air deflection)



- Air supply through **diffusers** (diffuses air)



**localized** air conditioning

heat extraction using: **refrigerant, water**



**Fancoils, indoor units** (air recirculation)



**Chilled beams** (active and passive)  
thermal conditioning +  
fresh air supply (active only)

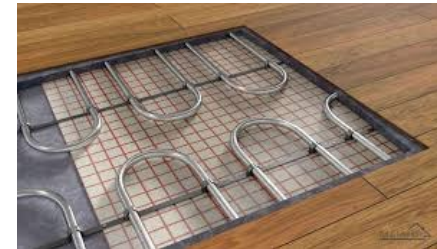
## Radiant systems

**centralized** water conditioning

heat extraction using: **water**



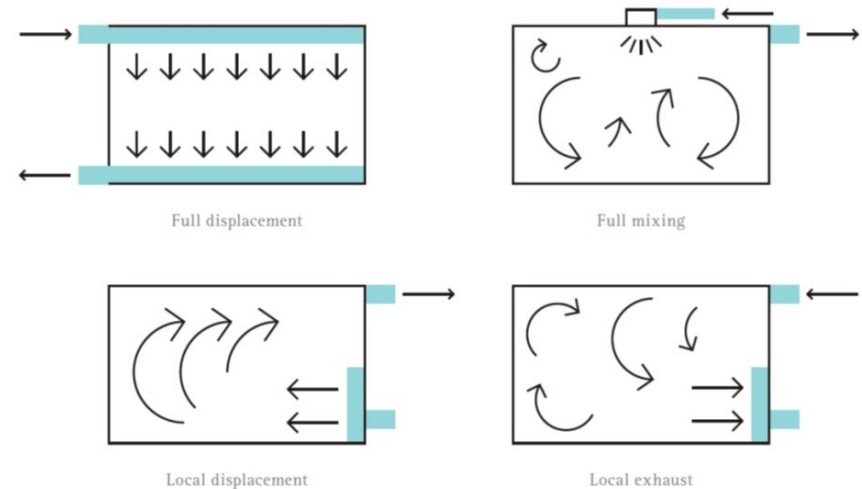
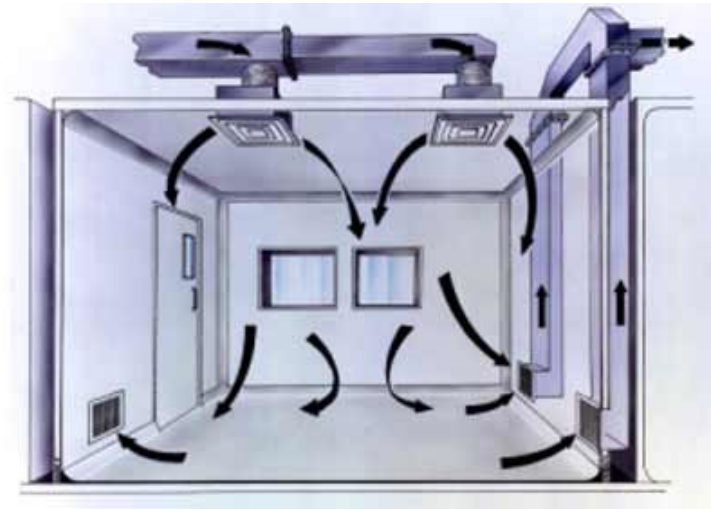
**Radiant ceiling**



**Floor/Wall systems**

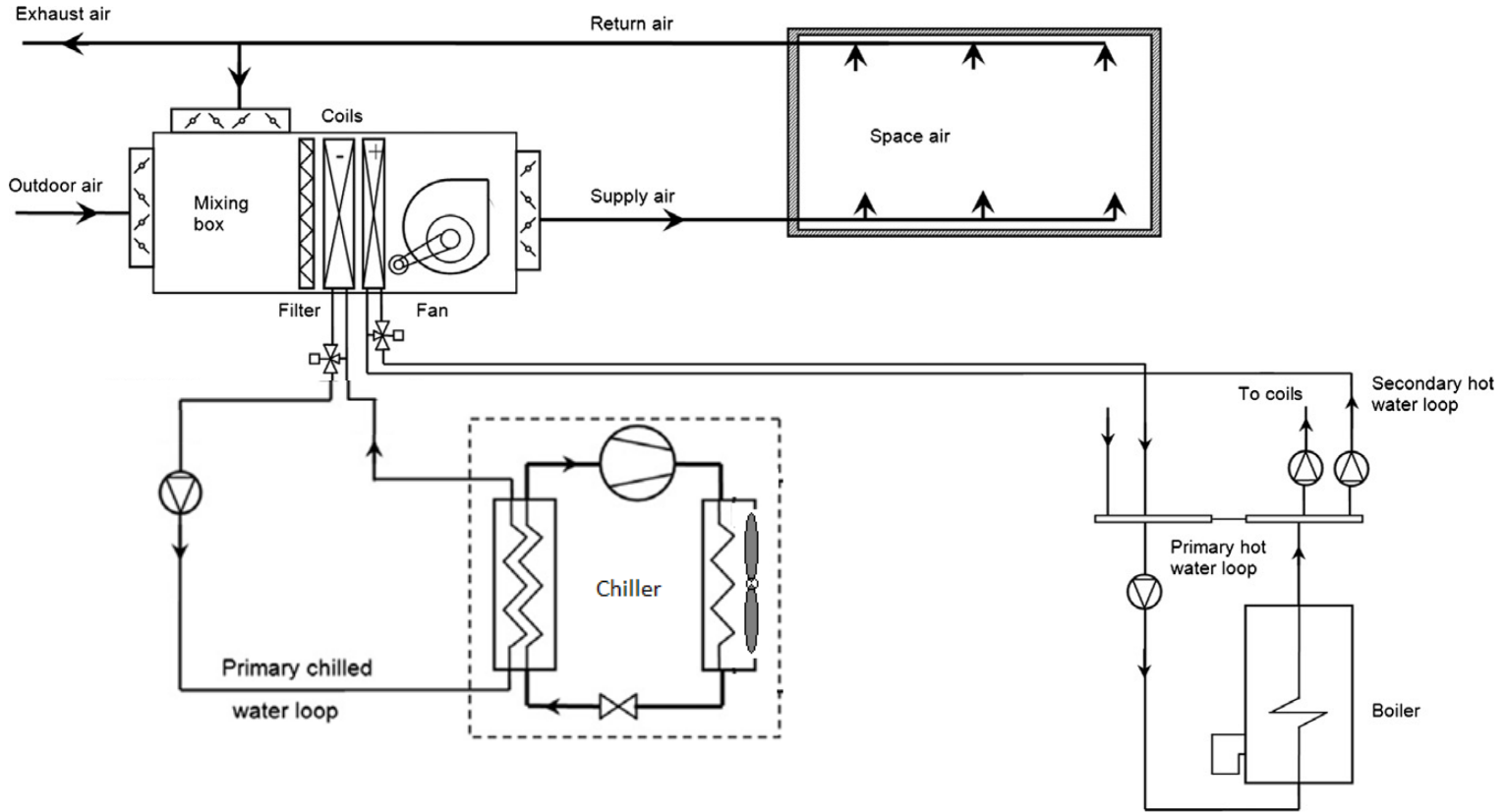
# Convective (All-Air) Systems

- A system where the **air** is used as **the heat carrier** (*medium of energy distribution*) and the **heat exchange** with **the conditioned space** is entirely by **convection**.
- Require **higher air flow rates** *than radiant systems* since **the entire heating/cooling load** needs to be addressed **by the ventilation system**
- **Types of systems:** mixing ventilation, displacement ventilation, underfloor air distribution, personalized ventilation, etc.
- Air can be **conditioned** in a **air-handling unit** using *various approaches* (electric heating, with hot water from a boiler or a heat pump, etc.)



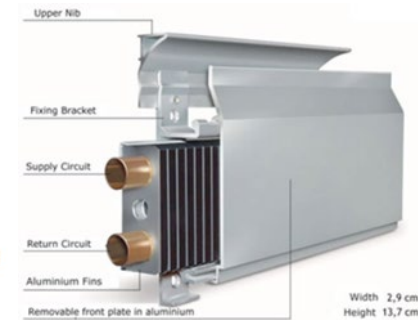
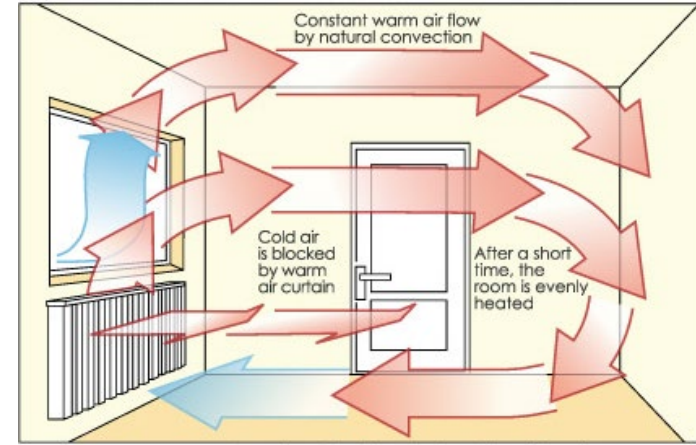


# Convective (All-Air) System: Supply Side



# Radiators/Convectors

- The **most conventional** heating practice
- **Types:** **electric** or **water-heated** (hot water circulates through pipes)
- **Heat transfer** mainly by **natural convection**
- **Fins** are used to *increase* the heat transfer area
- The **source of heat** is *not directly exposed* due to **aesthetic** and **safety** purposes
- **Configuration:** horizontal, column, towel radiators, etc.



Skirting boards (electric and water-based)



Baseboard radiator

# Steam Radiators

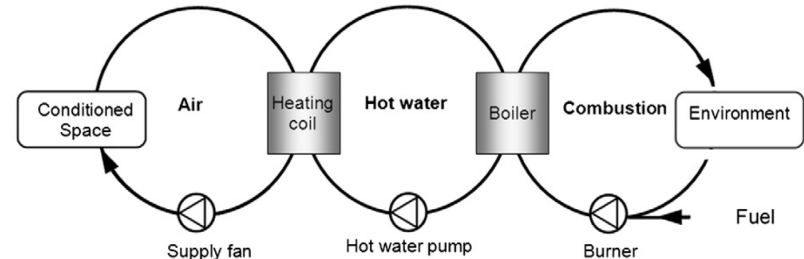
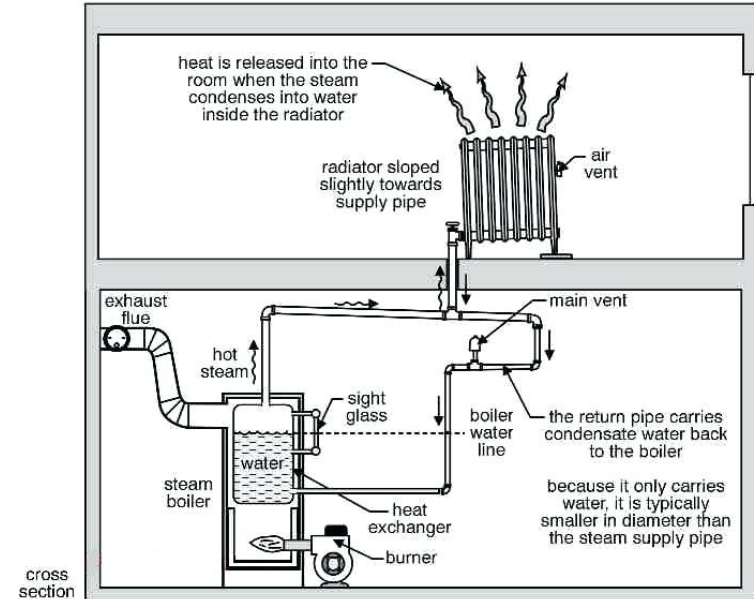
- One of the “oldest” heat emitting practices
- 1831**: AM Perkins (England) devised a high-pressure system of hot-water heating (steam at  $\sim 170^{\circ}\text{C}$  and pressure  $\sim 15$  atm)



Patent from 1867



## How steam systems work

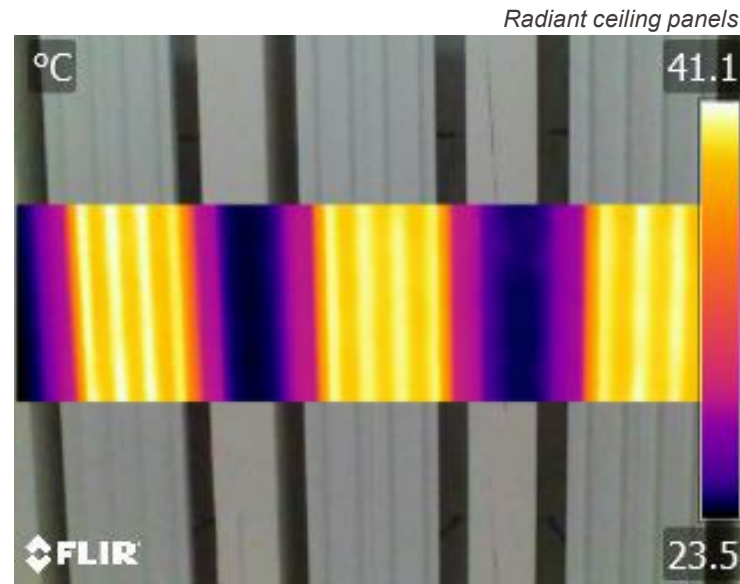


## “Steam” Radiators



- **Small** heat transfer area
- **Requires high water temperature ( $>50^{\circ}\text{C}$ )**
- Needs to be coupled **with high temperature water generation system** (district heating, boilers)
- **Non-uniform** indoor thermal environment

## Radiant Systems



- **Large** heat transfer area
- **Low temperature heating ( $30\text{--}40^{\circ}\text{C}$ )**
- Better **coupling with water generation systems coupled with renewable sources** (HPs, GHX)
- Provides **uniform** indoor environment



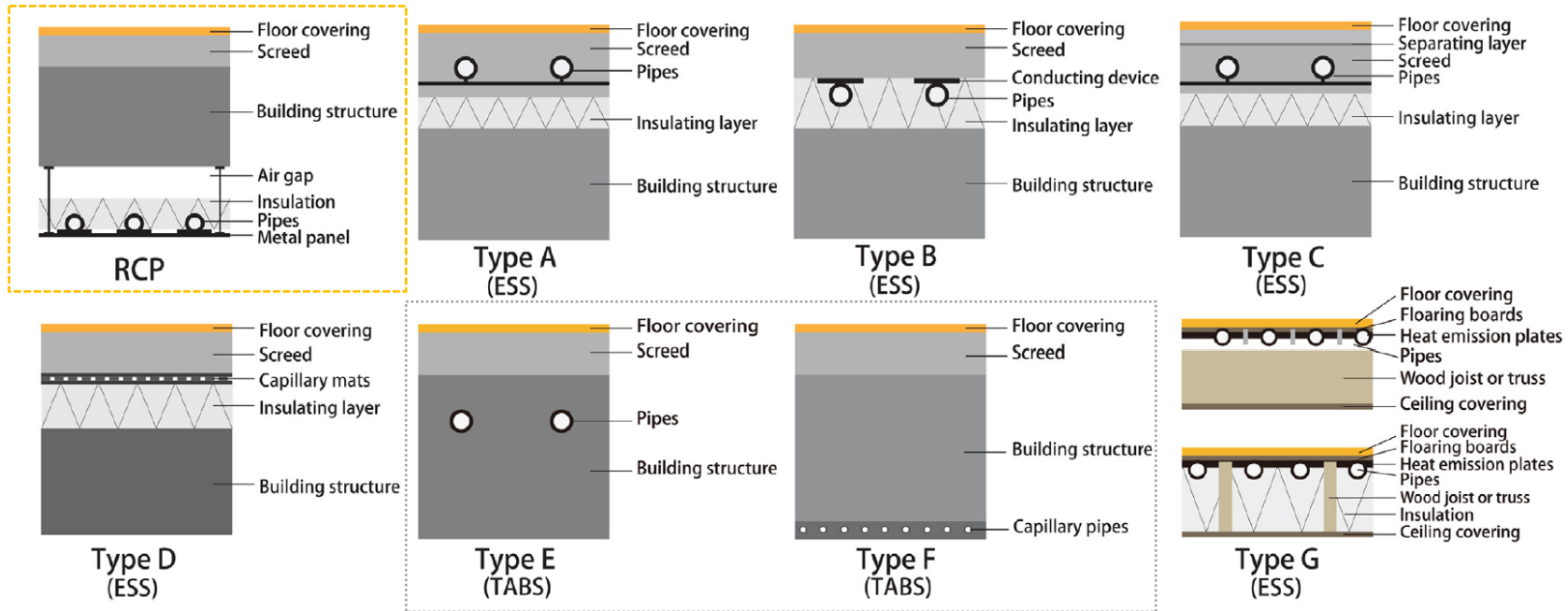
# EPFL Radiant Systems

- A system where typically **water** is used as **the heat carrier** (hydronic system) and **more** than  $\frac{1}{2}$  of the **heat exchange** with **the conditioned space** is by **radiation**.
  - Alternatively, **electric heaters** can also be used as *energy sources*.
- System consists of circuits of **water pipes embedded** in floor, wall or ceiling construction.
- Additional **ventilation system** is necessary *to address* the **latent loads** and to provide **the ventilation rates required** for **indoor air quality**.
- Radiant systems enable **lower air flow rates** than all-air convective systems.

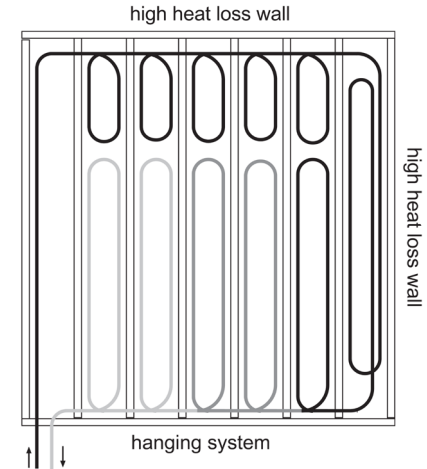
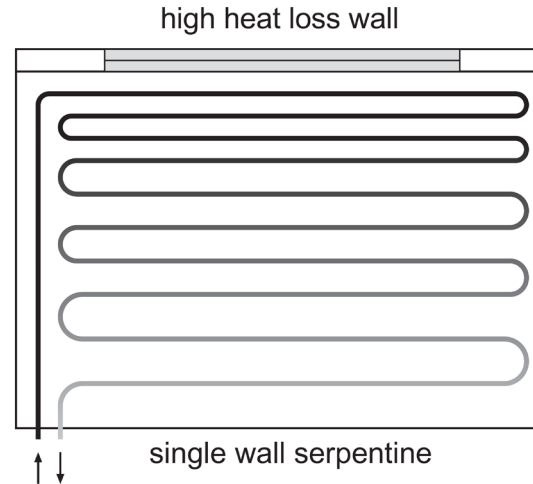
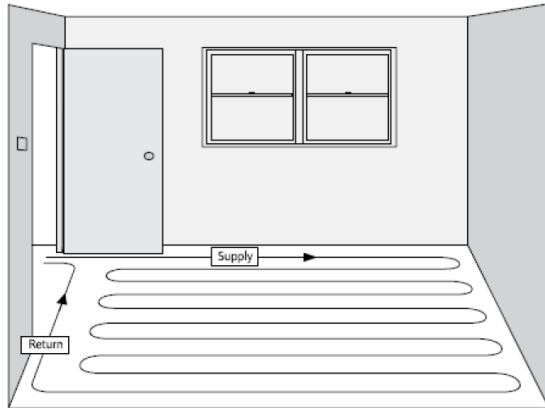


# EPFL Hydronic Radiant Systems: Typology

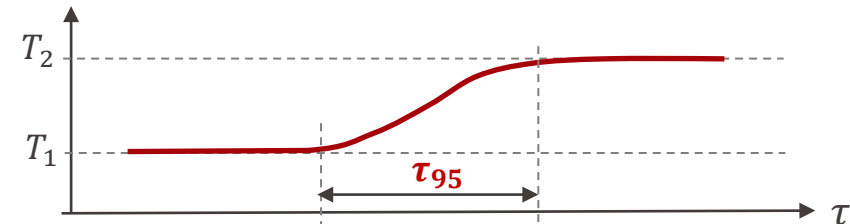
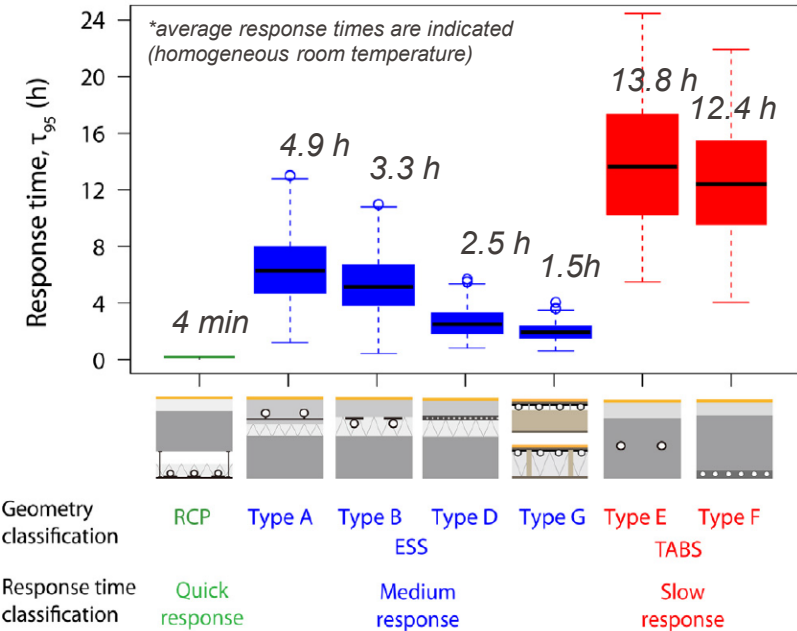
- Three main categories of hydronic systems:
  - radiant ceiling panels (RCP),
  - embedded surface systems (ESS)
  - thermally activated building systems (TABS)



- **Active surface area** - the surface area conditioned by the *embedded radiant system*
- The **layout of the piping** should consider *variable* heating and cooling demand, i.e., supply the hottest water to the zones with the highest heat losses
- **Water temperature** at the **inlet** corresponds to maximum circulating water temperature required to provide the maximum loads.
- **Piping layouts for floor systems** a single/double/triple-wall **serpentine**, a **counter flow**, and a **reverse-return**



- **Response Time** (a simple definition) – the time for the system to change from one *stable* condition to another
- **Response Time ( $\tau_{95}$ )** - the time it takes for the surface temperature of a radiant system **to reach 95%** of the **difference between its final and initial values** when a step change in control of the system is applied as input.
- **Determining parameters:**
  - **Geometric parameters**  
(pipe spacing; pipe diameter, concrete thickness, pipe-embedded depth)
  - **Thermal properties**  
(concrete type, floor covering material)
  - **Boundary conditions**  
(operative temperature, water temperature)





# EPFL Thermally Activated Building Systems (TABS)

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Assist. Prof. Dolaana Khovaylg

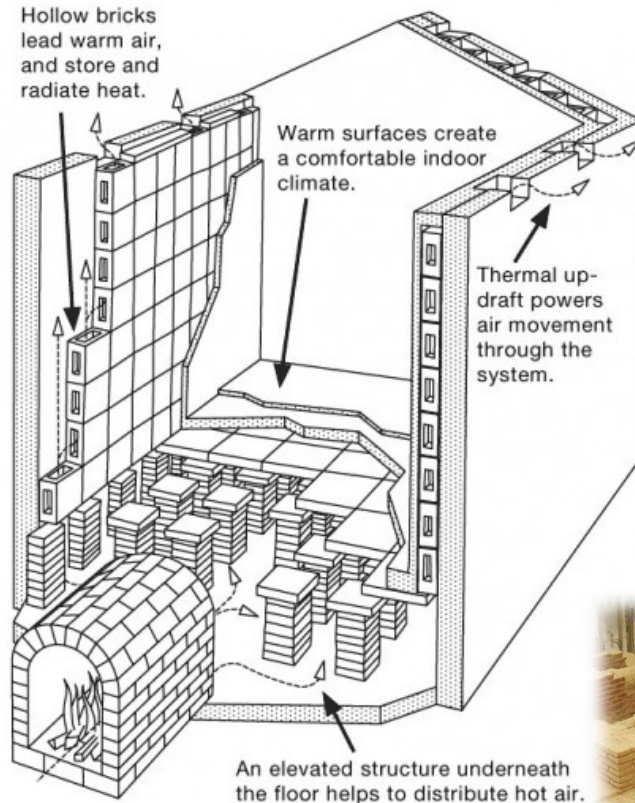


VS

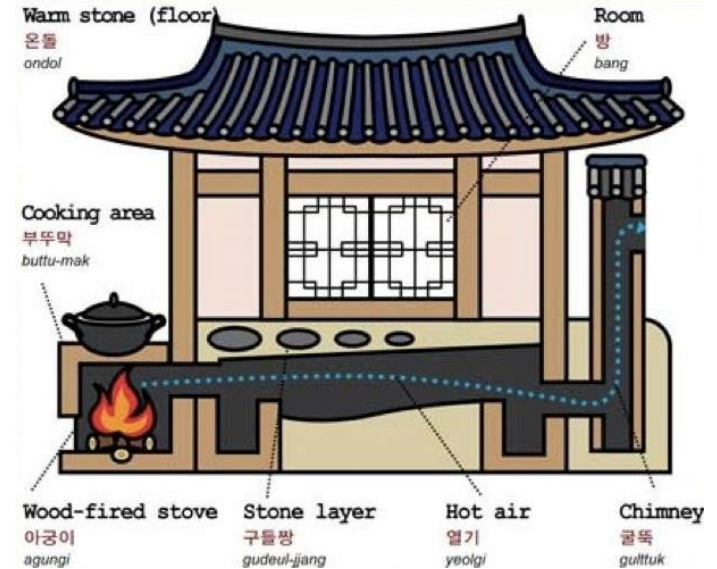


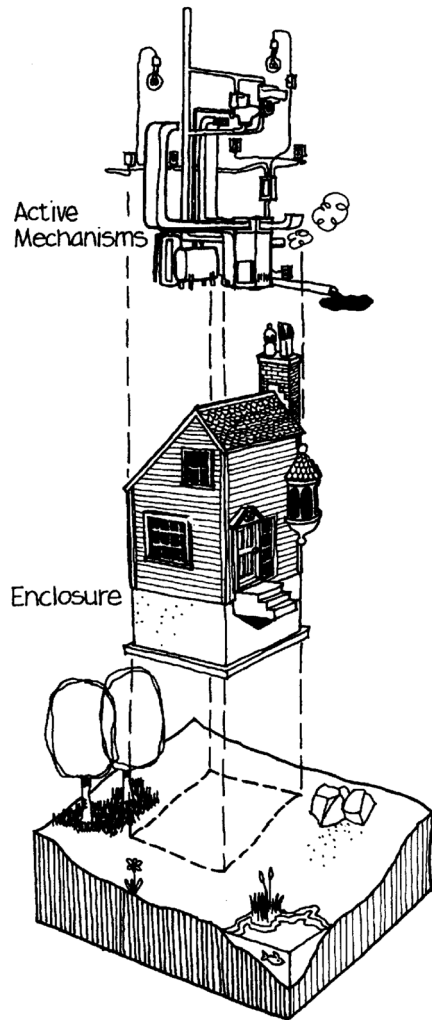
# Radiant Floor Heating: Old New?

## Roman Hypocaust heating (350 BC):



## Traditional Korean heating (Ondol, 5000 BC):





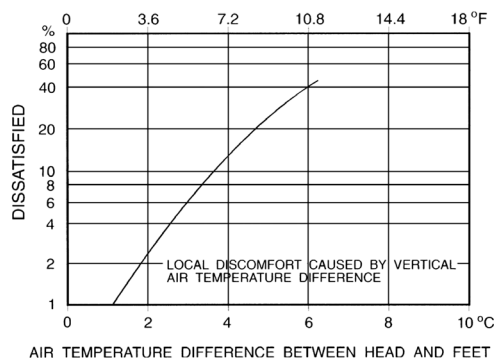
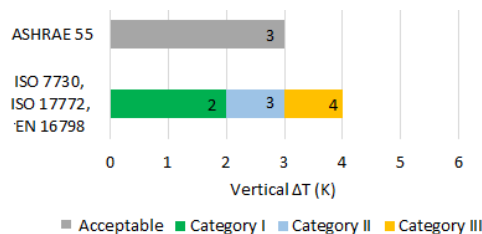
Source: Edward Allen «How Buildings Work» (2005)

# CONTENT:

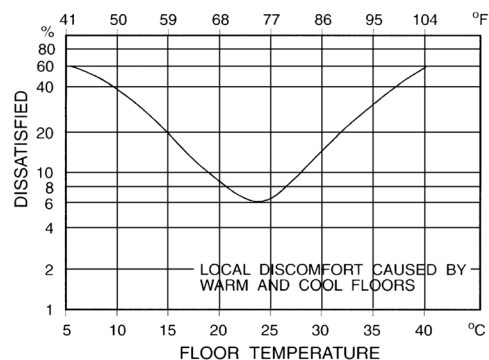
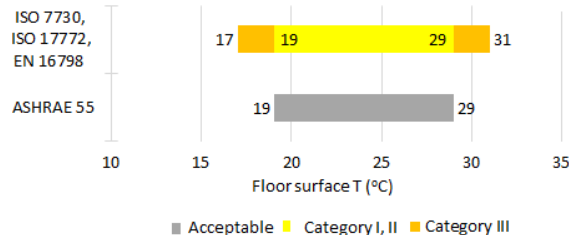
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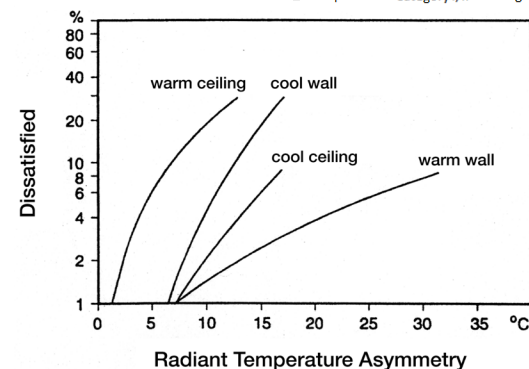
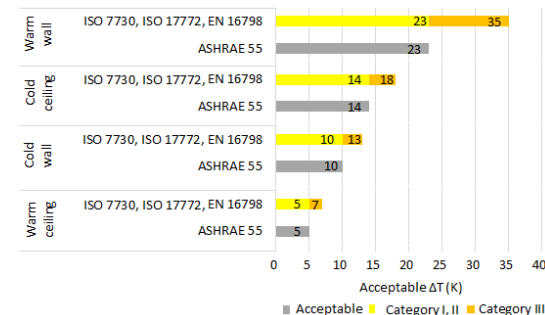
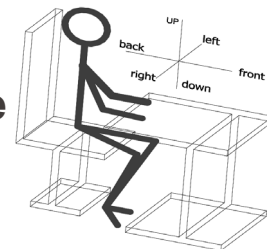
## Vertical Air Temperature Difference:



## Floor Surface Temperature:



## Radiant Temperature Asymmetry:

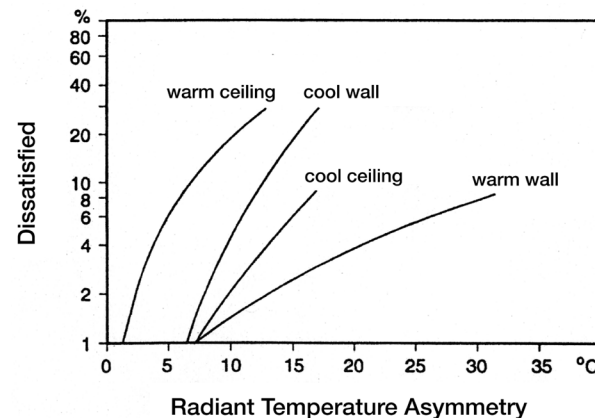
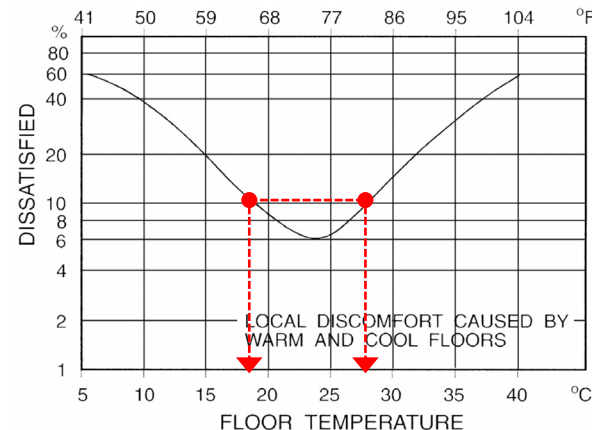




# EPFL Radiant Systems: Surface Temperature Limits

- The maximum surface temperature depends on the criteria for **radiant asymmetry** and **direct contact with the surface**
- Temperature limits **per ISO 7730** for surfaces (floor: occupants with normal shoes - Europe, America):  
**Floor: +29°C / Ceiling: +27°C / Walls: +40°C**
- Acceptable range for **floor surface** *should be adjusted for a certain lifestyle* (i.e., in Japan and Korea, occupants spend lots of time sitting on the floor):

ASHRAE Fundamentals handbook, 2009	According to the material of the floor	Textiles (rugs): 21≈28°C Pine floor: 22,5≈28°C Oak floor: 24,5≈28°C Hard linoleum: 24≈28°C Concrete: 26≈28,5°C	In America and Europe
Song, GS et al., 2001	According to the material of the floor	Clay: 24,9≈31,5°C Pine: 18,1≈29,0°C Urethane: 12,7≈23,2°C Veneer: 24,7≈31,0°C	In Korea
Ling Zhang et al.		Allowable range of floor surface temperature: 25≈31°C Comfortable range of floor surface temperature: 26≈30°C	In Japan



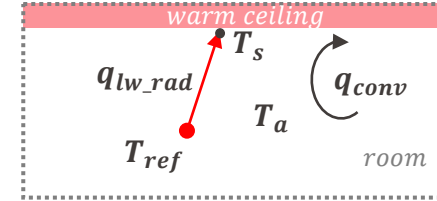
# EPFL Embedded Radiant Systems: **Rated Heat Flux**

- Surface convective heat transfer:
- Longwave radiation heat transfer:
- Total surface heat flux\*:  
(heat flow density, W/m<sup>2</sup>)

$$q''_{conv} = h_c \times (T_a - T_s)$$

$$q''_{lw\_surf} = h_{rad} \cdot (T_s - T_{ref})$$

$$q = h_t \cdot |T_s - T_{ref}|$$



$T_s = T_{m,s}$  mean surface temperature

$T_{ref} = T_{op}$  operative temperature (per ISO 18555)

- Heat transfer coefficient** between radiant surface and room condition:

Combined convection and (longwave) radiation heat transfer coefficient  $h_t$ :

Heating:		Cooling	
Floor heating (FH)	11 W/m <sup>2</sup> K	Floor cooling (FC)	7 W/m <sup>2</sup> K
Wall heating (WH)	8 W/m <sup>2</sup> K	Wall cooling (WC)	8 W/m <sup>2</sup> K
Ceiling heating (CH)	6 W/m <sup>2</sup> K	Ceiling cooling (CC)	11 W/m <sup>2</sup> K

Radiant (longwave) heat transfer coefficient  $h_{rad} = 5.5$  W/m<sup>2</sup>K  
(less than 4% error for surface temperatures in the range of 15-30°C)

- Heat flow density (W/m<sup>2</sup>):**  
at steady-state

- **floor heating** / **ceiling cooling**:  $q = 11 \cdot |T_{m,s} - T_{op}|$
- **wall heating** / **wall cooling**:  $q = 8 \cdot |T_{m,s} - T_{op}|$
- **ceiling heating**:  $q = 6 \cdot |T_{m,s} - T_{op}|$
- **floor cooling**:  $q = 7 \cdot |T_{m,s} - T_{op}|$

\* Shortwave radiation heat transfer **is not considered** in the *standard approach* of defining total heat flow density which might become problematic **for floor cooling** with direct sunlight

Source: ISO 11855-2:2012

What is the **comfort-related limiting heat flux** for **FLOOR** heating in the case of indoor operative temperature **20°C**?

- A. 80 W/m<sup>2</sup>
- B. 90 W/m<sup>2</sup>
- C. 100 W/m<sup>2</sup>
- D. None above

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What is the **comfort-related limiting heat flux** for **CEILING** heating in the case of **indoor operative temperature 20°C**?

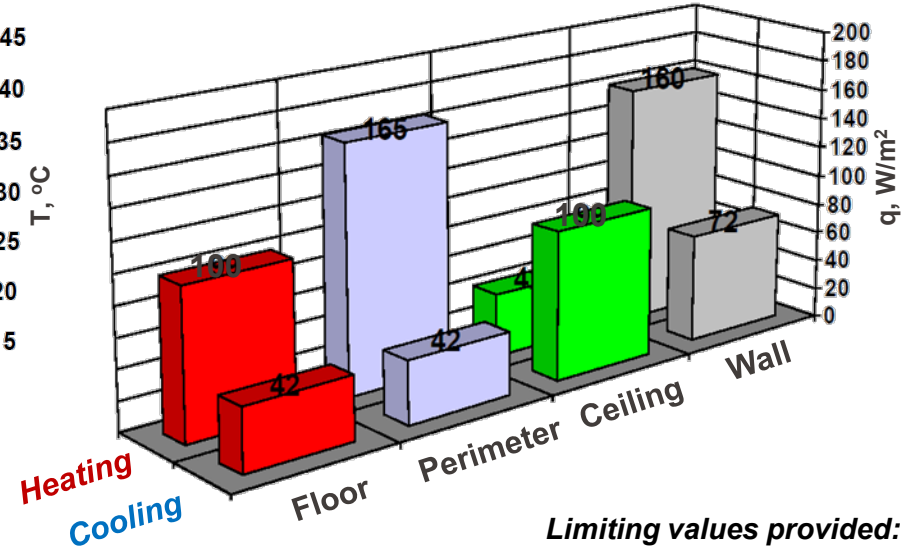
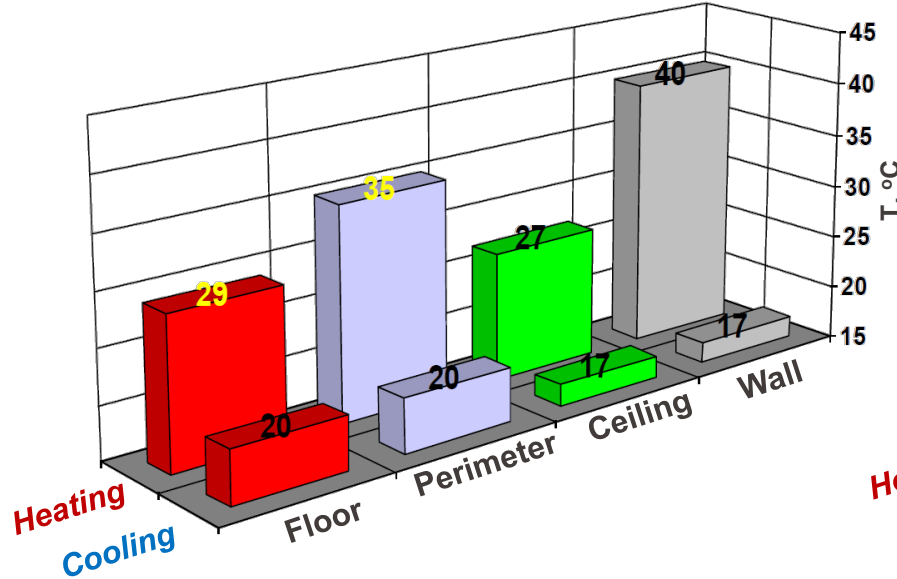
- A. 32 W/m<sup>2</sup>
- B. 42 W/m<sup>2</sup>
- C. 52 W/m<sup>2</sup>
- D. None above

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- **Maximum** heating and cooling capacity depends *on the position* of the radiant surface
- The heating/cooling capacity *is limited* by **relatively small convective heat transfer coefficient** between *the surface* and *air*, risk of condensation and concerns about surface temperature, radiant asymmetry, vertical air stratification and draft from comfort perspective



**Limiting values provided:**

- for **heating**:  $T_{op}=20^{\circ}\text{C}$
- for **cooling**:  $T_{op}=26^{\circ}\text{C}$

(for  $V_{air} < 0.2 \text{ m/s}$ )

- In heat exchangers, the heat transfer between **the hot stream** (water) and **the cold stream** (room air) occurs over **a finite area**  $A_s$  of the heat exchange.
- To determine the heat transfer  $Q$  [W] in heat exchangers, **LMTD method** can be used
  - $LMTD$  [K] - log-mean temperature difference
  - $U$  [ $W/m^2K$ ] – overall heat transfer coefficient

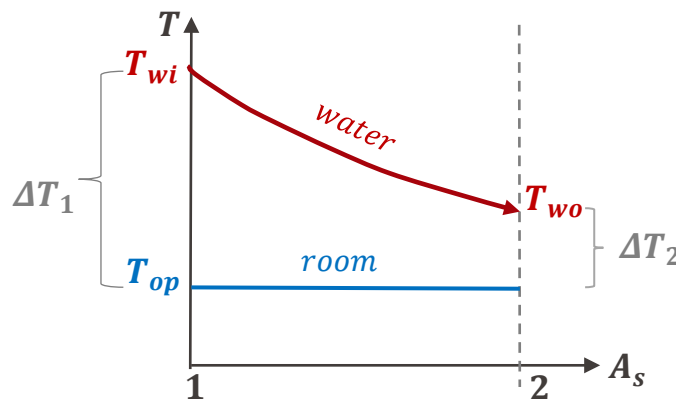
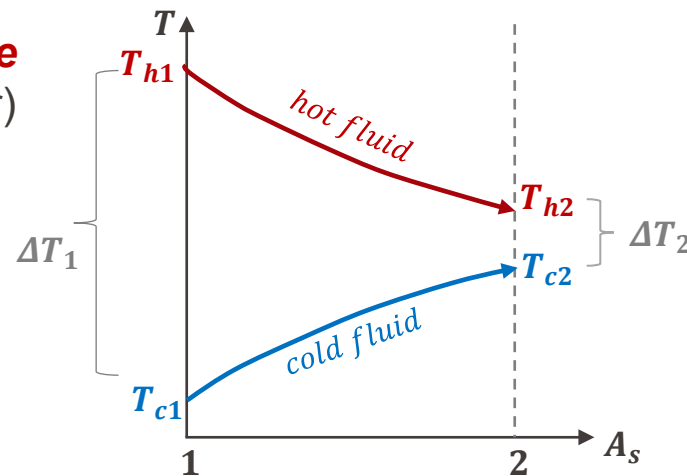
$$Q = U \cdot A_s \cdot \Delta T_{lm}$$

$$\Delta T_{lm} = \frac{\Delta T_1 - \Delta T_2}{\ln[\Delta T_1 / \Delta T_2]}$$

- $LMTD$  considering constant operative temperature  $T_{op}$  to be maintained indoors:

$$\Delta T_1 = T_{wi} - T_{op}, \quad \Delta T_2 = T_{wo} - T_{op}$$

$$\Delta T_{lm} = \frac{(T_{wi} - T_{wo})}{\ln[(T_{wi} - T_{op}) / (T_{wo} - T_{op})]}$$

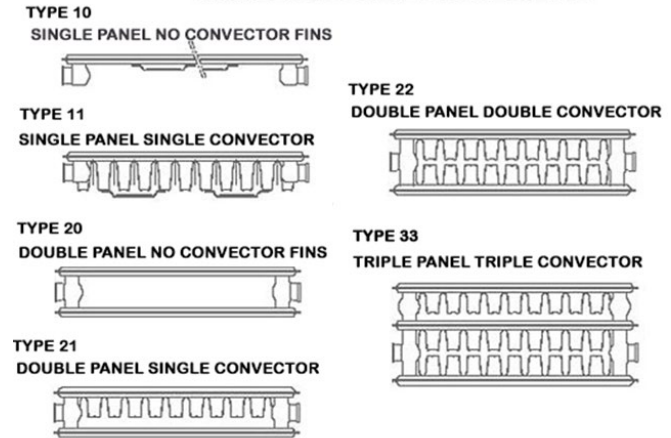


1. Determine the room peak heating demand  $Q_{demand}$
2. Measure the room size and space available
3. Choose type of the radiator (i.e., type 11, 22, 33, etc.)
4. Choose required device from a manufacturer's catalogues and determine  $Q_{fabricant}$  close to  $Q_{demand}$
5. Determine exponent  $n$  value indicated in the catalogue
6. Typical water temperature drop ( $T_{wi} - T_{wo}$ ) in radiators is limited to **10 K**
7. Determine water temperature using the following formulation considering (7):

$$Q_{demand} = Q_{fabricant} * \left( \frac{\Delta T_{actual}}{\Delta T_{standard}} \right)^n$$

where  $\Delta T_{actual} = \frac{(T_{wi} + T_{wo})}{2} - T_{room}$

$\Delta T_{standard} = 50K$  (see the catalogue)

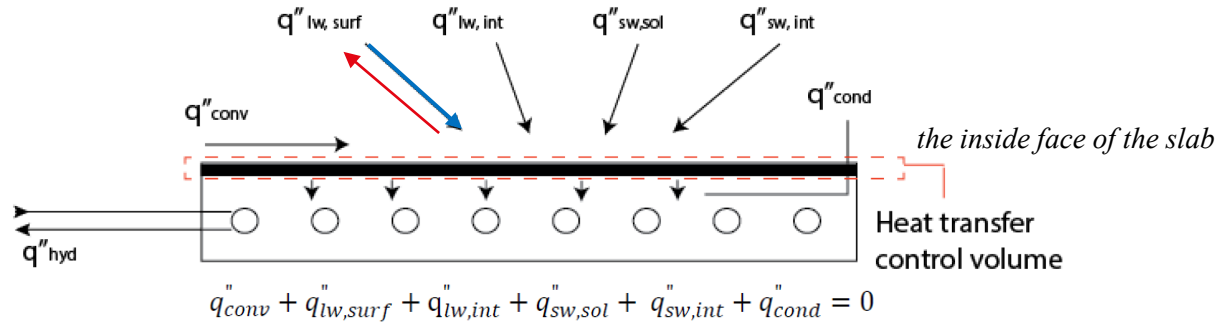


type 10		hauteur						
longueur	watt	300	400	450	500	600	750	900
450	$\Delta T 50$	145	186	206	225	263	318	370
600	$\Delta T 50$	193	248	275	301	351	424	493
750	$\Delta T 50$	242	310	344	376	439	530	617
900	$\Delta T 50$	290	372	412	451	527	635	740
1050	$\Delta T 50$	338	434	481	526	614	741	863
1200	$\Delta T 50$	386	496	550	601	702	847	986
1350	$\Delta T 50$	435	558	618	676	790	953	1110
1500	$\Delta T 50$	483	620	687	752	878	1059	1233
1650	$\Delta T 50$	531	681	756	827	965	1165	1356
1800	$\Delta T 50$	580	743	824	902	1053	1271	1480
EN 442 - 75/65/20°C		322	413	458	501	585	706	822
EN 442 - 90/70/20°C		411	526	584	638	745	899	1046
valeur n		1,3325	1,3307	1,3297	1,3288	1,3270	1,3242	1,3215

Source: <https://www.radson.com/docs/Radson-Fiche-technique-CLD-FR.pdf>

Source: <http://cruzoe.free.fr/enr/donn%E9es%20diverses/Les%20radiateurs%20Calculs.pdf>

- Two heat transfer (HT) processes involved:
  - HT *between the surface of the radiant layer and the space* it is conditioning
  - The HT *between the radiant layer and the water loop*



The amount of **heat supplied** by an **activated heating surface** is a **combination** of *convection* and *radiation*:

$$q''_{surf} = -q''_{cond} = q''_{conv} + q''_{lw,surf} + q''_{lw,int} + q''_{sw,sol} + q''_{sw,int} = q''_{conv} + q''_{rad\_surf}$$

$$q''_{hyd} = (\dot{m}c_p)_{water}(T_{wi} - T_{wo})$$

 $\dot{m}$ 

= Mass flow rate of water, kg/s;

 $c_p$ 

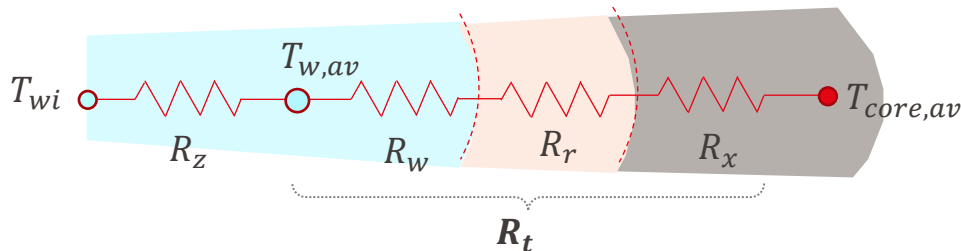
= Specific heat of water J/kg · K;

 $T_{wi}, T_{wo}$ 

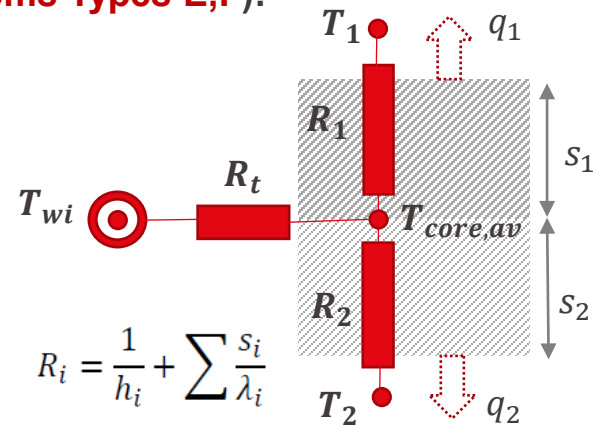
= Supply and return water temperature respectively, °C.



- Conduction heat transfer is *the major* heat transfer mechanism **between the surfaces and the hydronic loop** once *heat has been absorbed* by the radiant surfaces
- Thermal resistance network in the slab and between the slab and water loop is used to solve the conduction problem to determine the cooling/heating capacity for **Type E** and **F** systems
- Heating capacity estimation using resistance method (**systems Types E,F**):



- $R_t$  - total resistance between the heat source and the conducting layer
- $R_z$  - resistance between the supply water at temperature  $T_{wi}$  and the average water at temperature  $T_{w,av}$
- $R_w$  - resistance between water at average temperature  $T_{w,av}$  and internal wall surface of the pipe ( $1/h_w$ )
- $R_r$  - resistance between water and the outside pipe wall
- $R_x$  - resistance between the pipe outside wall temp. and the conductive layer (a fictive core) at average temp. of  $T_{core,av}$
- $R_i$  - thermal resistance *in the heat-conducting layer* (from the heat-conducting plate to the room *above* "1" or *below* "2")



$$R_i = \frac{1}{h_i} + \sum \frac{S_i}{\lambda_i}$$

$$q'' = K_H \cdot \Delta T_h$$

$$K_H = 1/(R_t + R_i)$$

## ■ Universal power law (for embedded systems **Type A, B, C, D**):

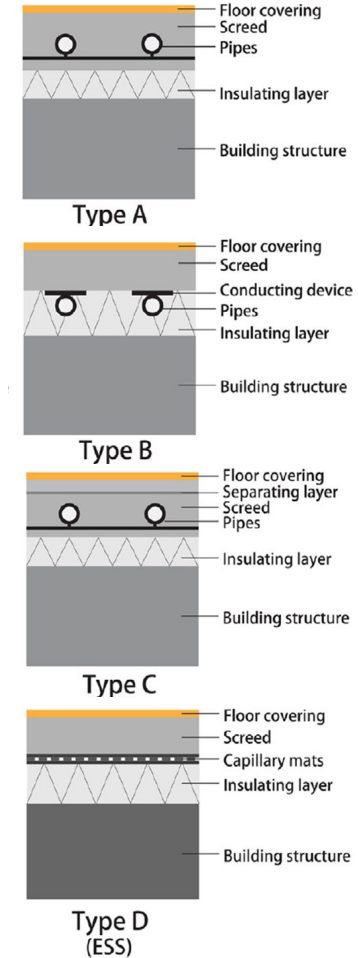
- **Heat flux at a surface:**  $q'' = K_H \cdot \Delta T_h^n$  , where  $1 < n < 1.05$
- **Mean temperature difference** between heat carrier (water) and the space:

$$\Delta T_h = \frac{(T_{wi} - T_{wo})}{\ln \left[ (T_{wi} - T_{op}) / (T_{wo} - T_{op}) \right]}$$

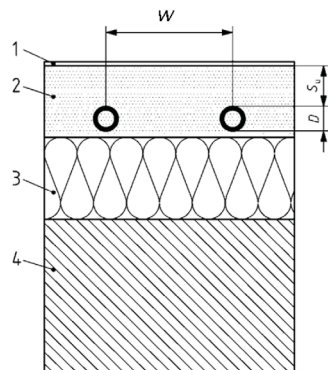
- **Lumped thermal resistance:**  $K_H = B \cdot \prod (a_i^{m_i})$

system dependent  
coefficient,  $W/(m^2K)$

a power product linking  
parameters of the structure



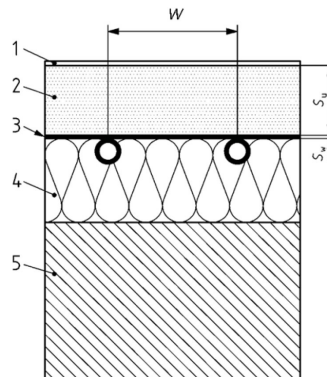
## Systems Types A, C:



$$q = B \cdot a_B \cdot a_W^{m_w} \cdot a_U^{m_u} \cdot a_D^{m_D} \cdot \Delta T_h$$

$$B = 6.7 \text{ W/(m}^2\text{K)}$$

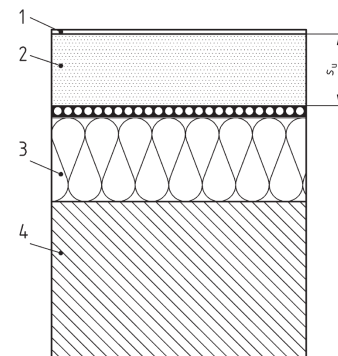
## System Type B:



$$q = B \cdot a_B \cdot a_W^{m_w} \cdot a_U \cdot a_{WL} \cdot a_K \cdot \Delta T_h$$

$$B = 6.5 \text{ W/(m}^2\text{K)}$$

## System Type D:



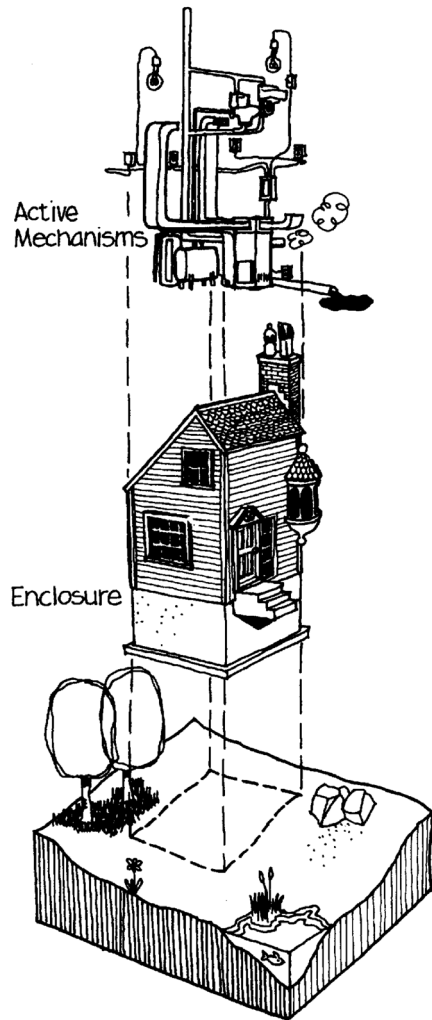
$$q = B \cdot a_B \cdot a_W^{m_w} \cdot a_U \cdot \Delta T_h$$

$$B = 6.5 \text{ W/(m}^2\text{K)}$$

- $a_B$  - surface covering factor
- $a_W$  - the pipe spacing factor,  $f(R_{\lambda,B})$
- $a_U$  - the screed covering factor,  $f(W, R_{\lambda,B})$
- $a_D$  - the pipe external diameter factor,  $f(W, R_{\lambda,B})$
- $a_B$  - heat conduction device factor,  $f(K_{WL}, W, D)$
- $a_K$  - correction factor for the contact,  $f(W)$

*Values are  
tabulated in  
ISO 11855*

- Factor considering spacing of pipes:  
 $m_w = 1 - W/0.075$
- Factor considering covering thickness:  
 $m_u = 100 \cdot (0.045 - s_u)$
- Factor considering diameter of pipes:  
 $m_D = 250 \cdot (D - 0.020)$



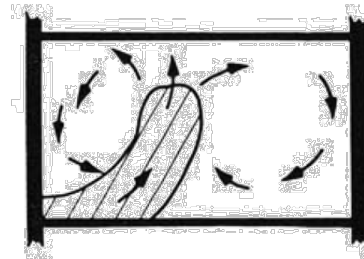
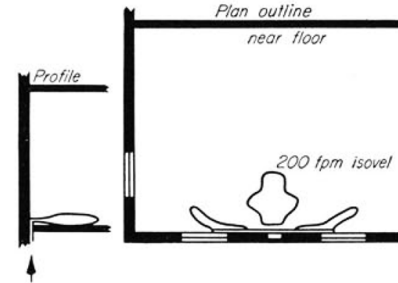
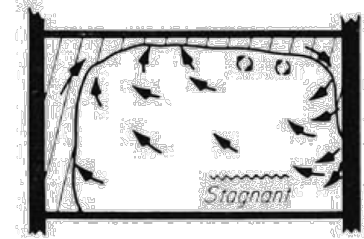
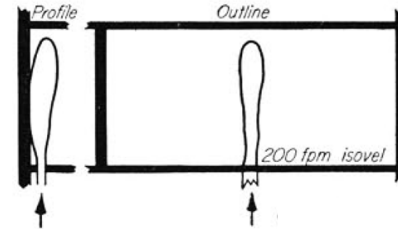
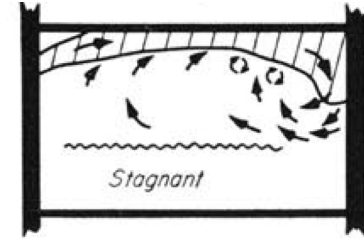
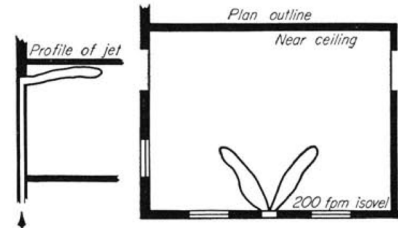
Source: Edward Allen «How Buildings Work» (2005)

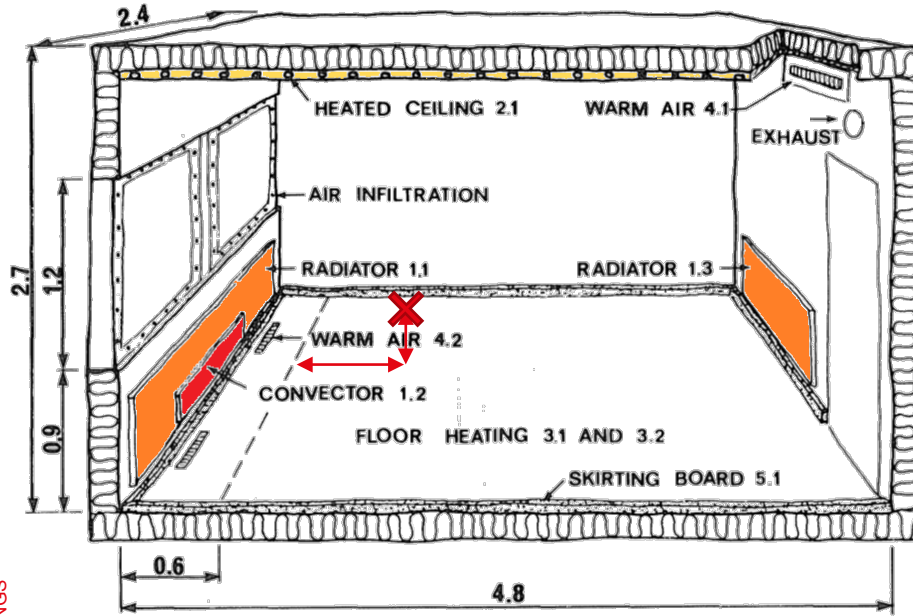
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## Distinct groups of air patterns:

- Air is discharged at the ceiling level
- Air is discharged vertically from floor grill (non-spreading floor outlet)
- Air spread horizontally across the floor (long baseboard units that spread air over a wide floor area)





- Test room:  $4.8 \times 2.4 \times 2.7 \text{ m}^3$
- Outside air temperature simulation:  $-5^\circ\text{C}$  and  $+4^\circ\text{C}$  (only for the front wall with windows)
- Multiple space heating approaches **comparison** for **PMV=0** condition *at the reference point* (1 m away from window at the height of 0.6 m)

Sources: Olesen B. W. et al. (1978). *Thermal comfort in a room heated by different methods*

No	Emission	Description	Heat carrier	$T_{\text{supply}} (^\circ\text{C})$
1.1	Radiator	Single panel radiator beneath the window covering most of the lower wall	Warm water	37-48
1.2	Convector	3 panel convectors beneath the window	Warm water	39-53
1.3	Radiator	Single panel radiator at the back wall	Warm water	46-63
2.1	Ceiling	Aluminium plates with water-filled coils, supply along the frontage and return at the back wall	Warm water	34-42
3.1	Floor (uniform)	Electrical heating foil covered by a 2 mm aluminium plate (uniform distribution)	El. Heater	--
3.2	Floor (non-unif)	As 3.1, but the effect on a 0.6 m strip along the frontage was higher ( $T_{\text{surf}}=29^\circ\text{C}$ )	El. heater	--
4.1	Warm air	Outlet in the back wall near the ceiling, 4 ACH, $V=1.2 \text{ m}^3/\text{s}$ .	Warm air	34-43
4.2	Warm air	2 outlets in the floor beneath the window, 4 ACH, $V=1.2 \text{ m}^3/\text{s}$ .	Warm air	34-43
5.1	Skirting board	Small electrical heated panels along the periphery of the room	El. heater	--

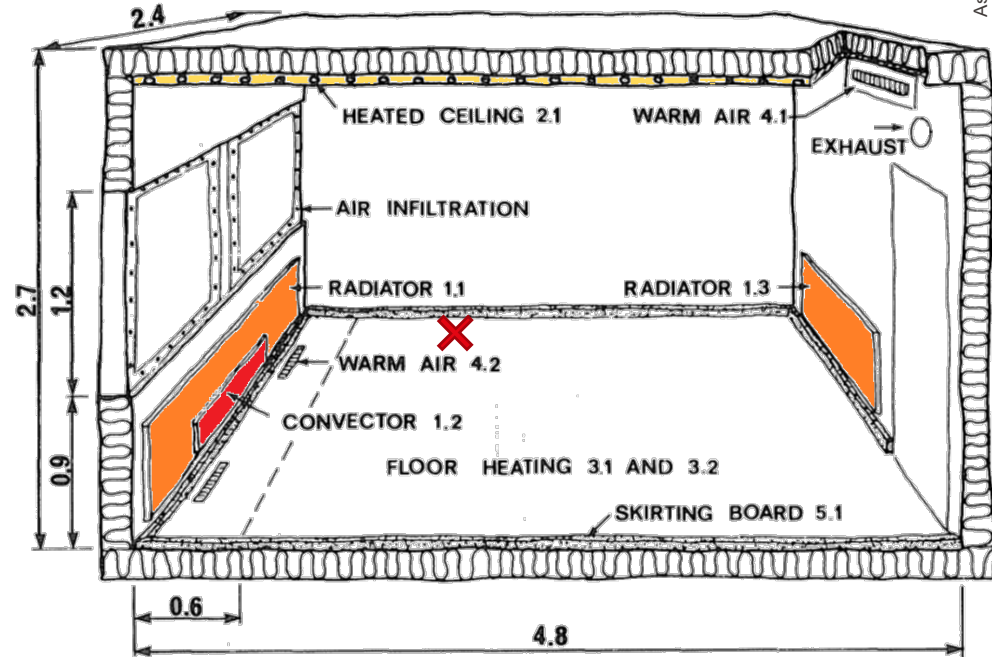
What **type of system** would lead to the **highest vertical air temperature difference** at the reference point (X)?

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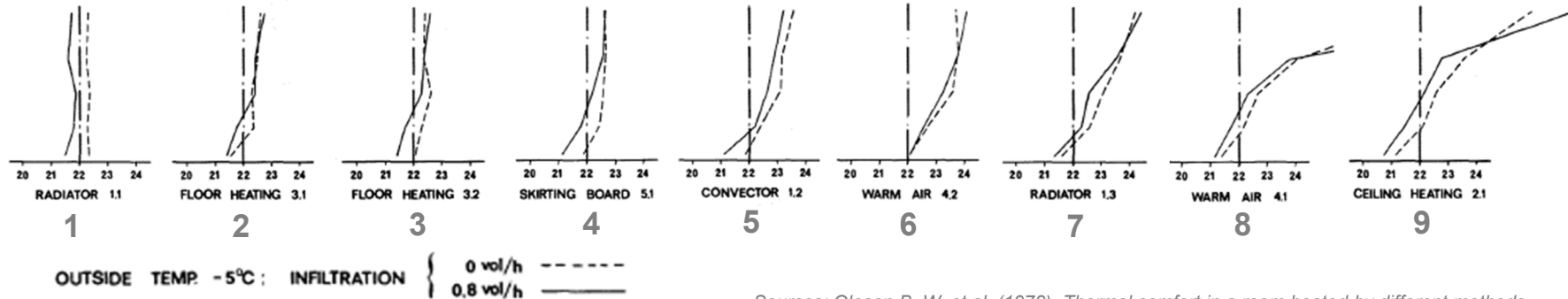
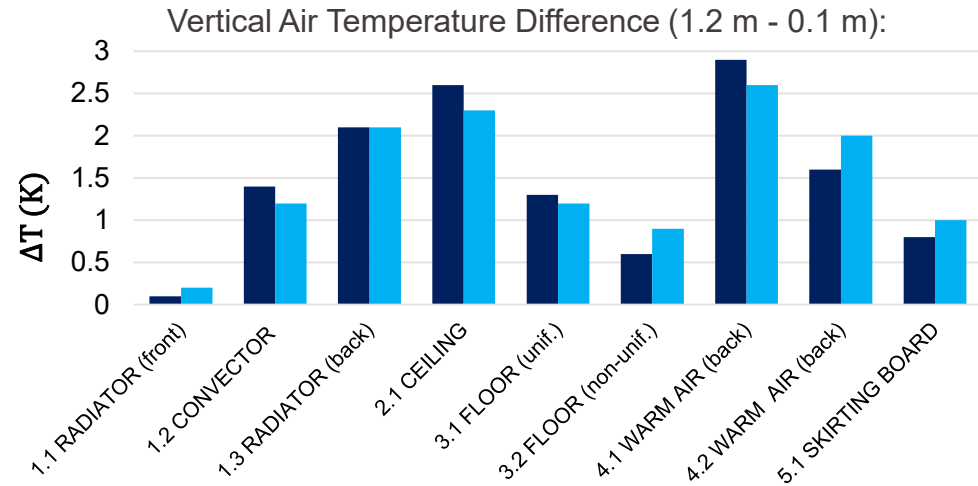
[responseware.eu](https://responseware.eu)

Session ID: **ENG445**

- A. Radiator (1.3)
- B. Warm air (4.1)
- C. Warm air (4.2)
- D. Heated ceiling (2.1)



- The *highest vertical air temperature difference (0.1-1.8m)* is for **warm air system (4.1)** with outlet in the back wall near the ceiling, and a **heated ceiling (2.1)**
- *Increased air infiltration rate decreased vertical air temperature difference slightly*





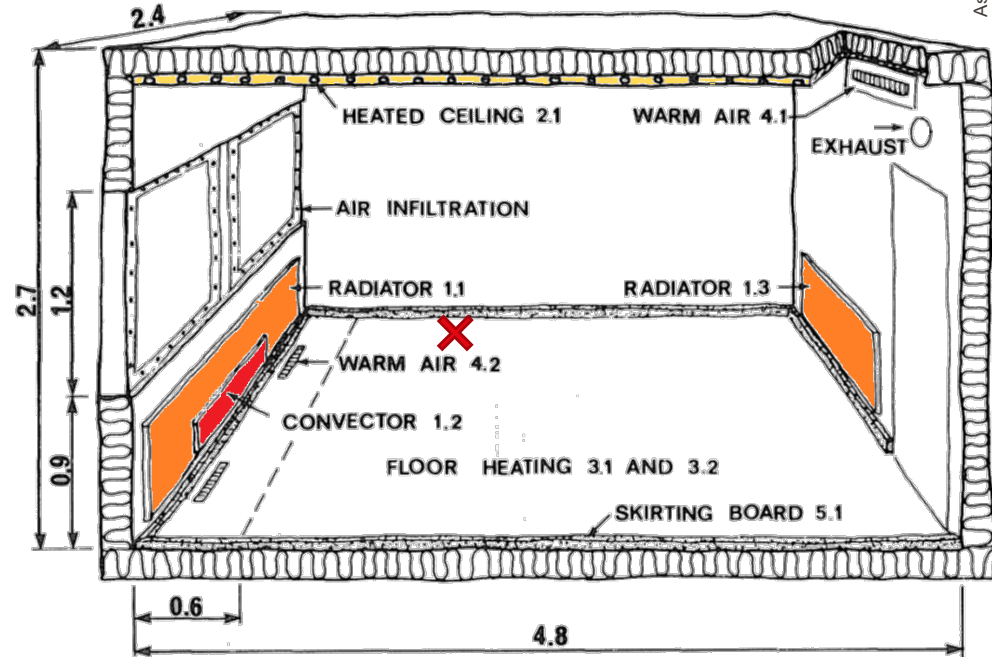
What type of system would lead to the highest **VERTICAL** radiant temperature asymmetry at the reference point (X)?

Please login:

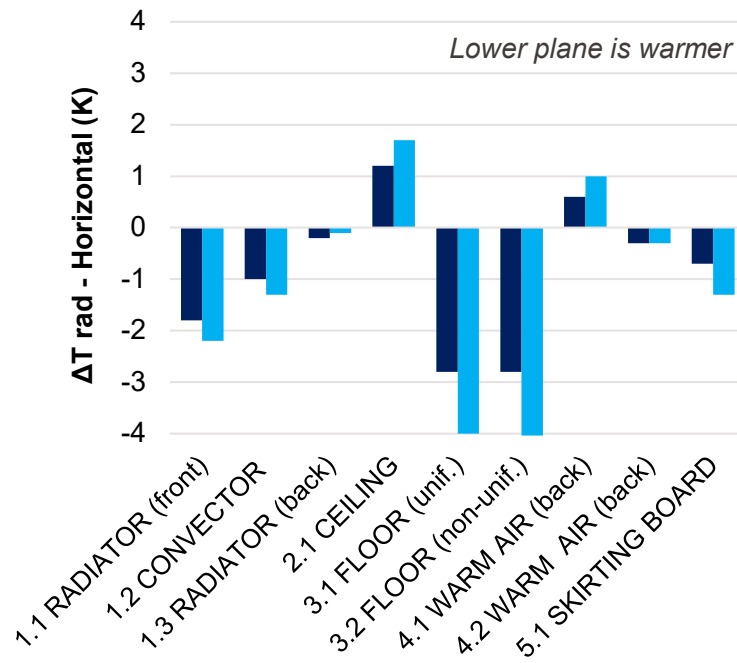
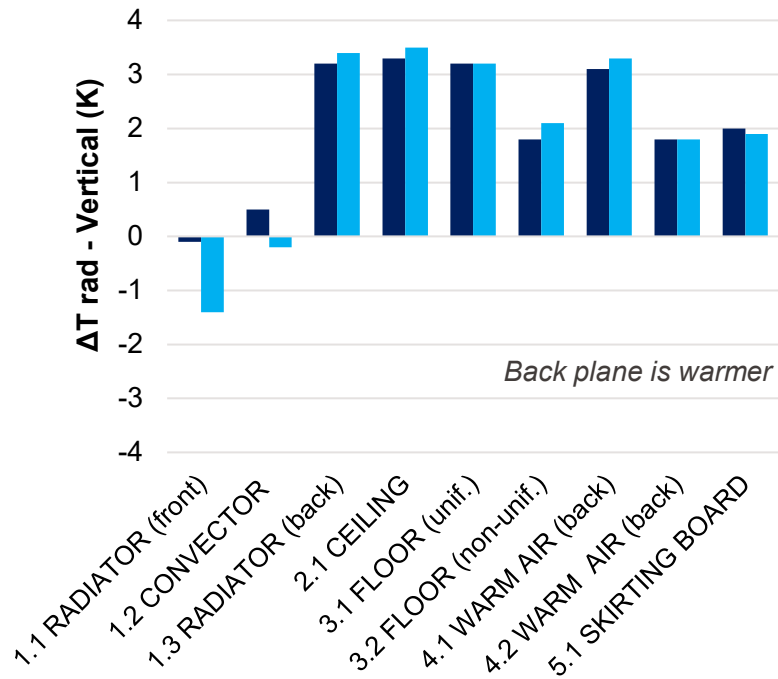
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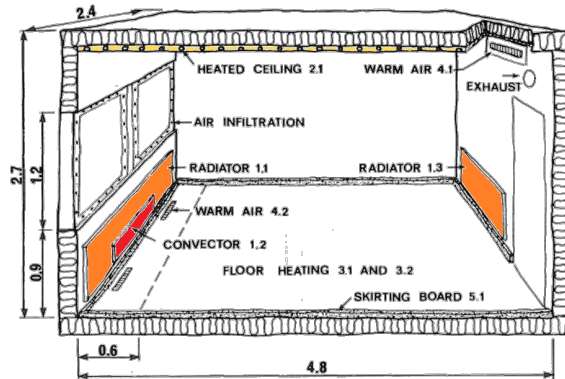
- A. Radiator (1.3)
- B. Warm air (4.1)
- C. Warm air (4.2)
- D. Heated ceiling (2.1)



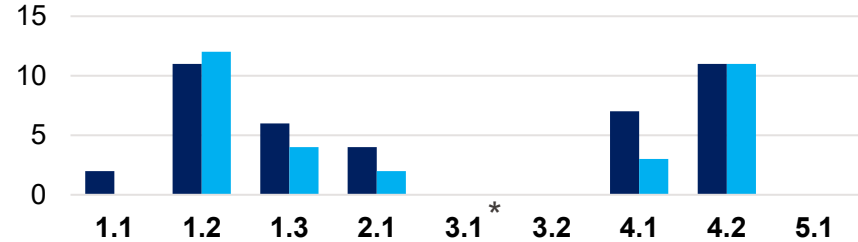
## Radiant Temperature Asymmetry (Vertical & Horizontal Plane):



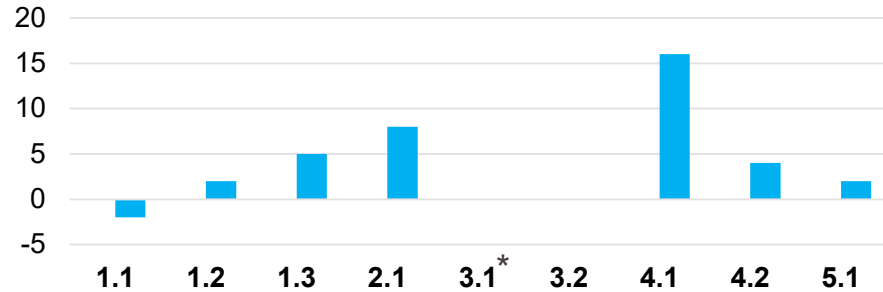
- **Total heat losses:** *the lowest* for the floor heating system (3.1)
- **The heat loss through the window:** *the highest* for **convector** (1.2) and **warm air** (4.2) due to *increased air velocity and air temperature* along the window surface (upward natural/forced convection)
- **The heat loss by infiltration:** *the highest* with **warm air** (4.1) system *with air supply from the back*



Heat losses through the window (in %):



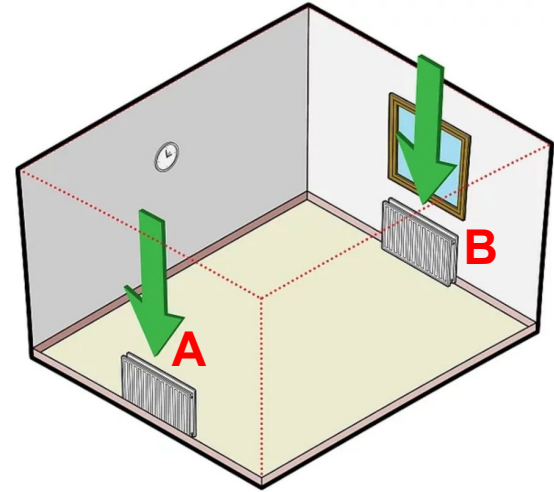
Heat losses by infiltration (in %):



\* Uniform floor heating (3.1) is considered as the baseline

# What is the **optimal location** of the **radiator** from **comfort** and **energy perspective**?

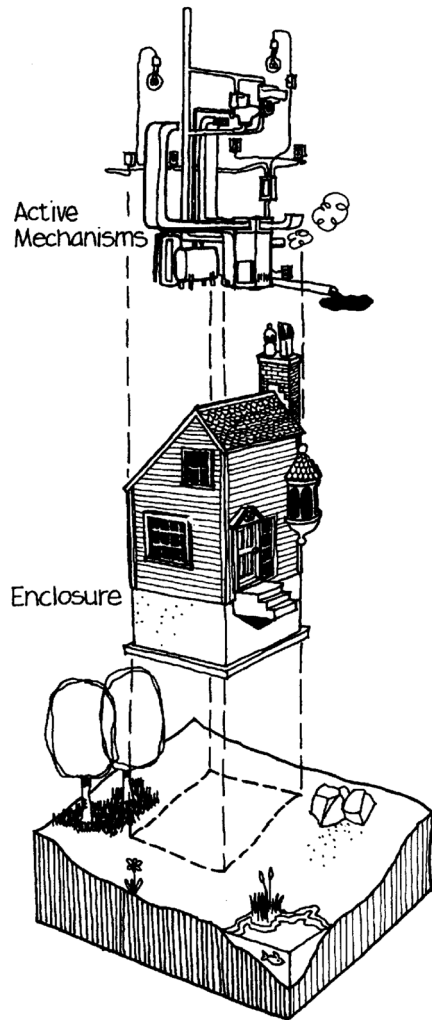
- A. A
- B. B
- C. Need more information to answer



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Source: Edward Allen «How Buildings Work» (2005)

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# EPFL Standards: Heating Load, Emission and Generation

Code	Title
EN 12831-1:2017	Energy performance of buildings - Method for calculation of the design heat load – <b>Part 1: Space heating load</b>
EN 12831-3:2017	Energy performance of buildings - Method for calculation of the design heat load – <b>Part 3: Domestic hot water systems heat load and characterization of needs</b>
EN 15316-2:2017	Energy performance of buildings - Method for calculation of system energy requirements and system efficiencies – <b>Part 2: Space emission systems (heating and cooling)</b>
EN 15316-3:2017	Energy performance of buildings - Method for calculation of system energy requirements and system efficiencies – <b>Part 3: Space distribution systems (DHW, heating and cooling)</b>
EN 15316-4-1:2017	Energy performance of buildings - Method for calculation of system energy requirements and system efficiencies – <b>Part 4-1: Space heating and DHW generation systems, combustion systems (boilers, biomass)</b>

## Swiss Regulations:

SIA 380:2015	Bases pour les calculs énergétiques des batiments
SIA 384.201:2017	Performance énergétique des bâtiments - Méthode de calcul de la charge thermique nominale - Partie 1: Charge de chauffage des locaux, module M3-3
SIA 380/1:2016	Besoins de chaleur pour le chauffage

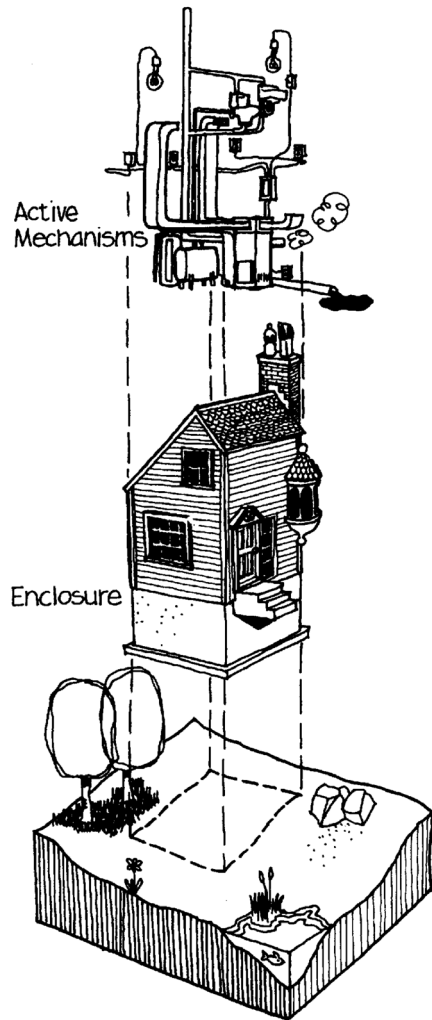
# EPFL Standards: Radiators and Hydronic Radiant Panels

Code	Title
EN 442-1:2014	Radiators and convectors - Part 1: Technical specifications and requirements
EN 442-2:2014	Radiators and convectors - Part 2: Test methods and rating

Code	Title
ISO 18566-1:2017	Building environment design — Design, test methods and control of <b>hydronic radiant heating and cooling panel systems — Part 1: Vocabulary, symbols, technical specifications and requirement</b>
ISO 18566-2:2017	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 2: Determination of heating and cooling capacity of ceiling mounted radiant panels</b>
ISO 18566-3:2017	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 3: Design of ceiling mounted radiant panels</b>
ISO 18566-4:2017	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 4: Control of ceiling mounted radiant heating and cooling panels</b>
ISO 18566-6:2019	Building environment design — Design, test methods and control of hydronic radiant heating and cooling panel systems — <b>Part 6: Input parameters for the energy calculation</b>

Code	Title
ISO 11855-1:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 1: Definition, symbols, and comfort criteria</b>
ISO 11855-2:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 2: Determination of the design heating and cooling capacity</b>
ISO 11855-3:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 3: Design and dimensioning</b>
ISO 11855-4:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 4: Dimensioning and calculation of the dynamic heating and cooling capacity of Thermo Active Building Systems (TABS)</b>
ISO 11855-5:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 5: Installation</b>
ISO 11855-6:2012	Building environment design — Design, dimensioning, installation and control of embedded radiant heating and cooling systems — <b>Part 6: Control</b>





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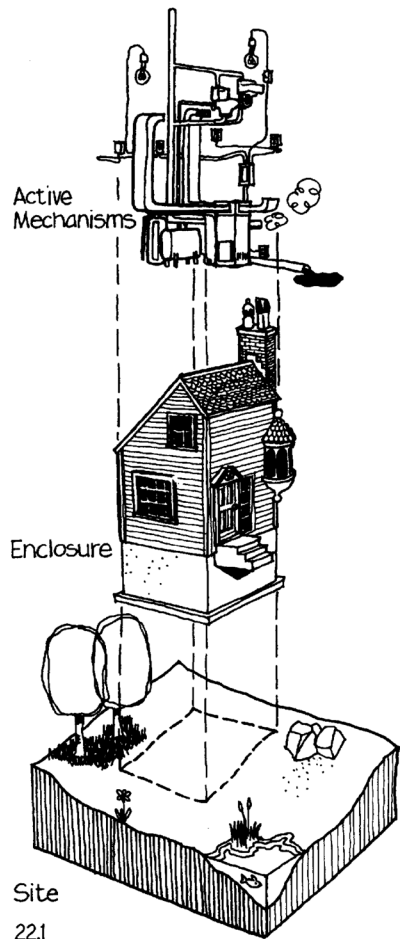
- **Heating/Cooling Emission Systems Overview**

Role of emission systems within active heating and cooling systems.

- **Heating Emission Systems Categorization**

Types of systems: **All-air systems**, **radiators (convectors)**, and **radiant systems**.

- **All-Air Systems:** Definition, key characteristics, and configuration options.
- **Radiators/Convectors:** Definition, main features, and common setup types.
- **Radiant Systems:** Definition, attributes, layout designs, and key considerations.
- **Types of Radiant Systems:** Radiant Ceiling Panels (RCP), Embedded Surface Systems (ESS), and Thermally Activated Building Systems (TABS)
- **Local Thermal Discomfort Overview**  
Impact of radiant asymmetry and surface temperature limits on comfort.
- **Technical Overview/Considerations:** Heat transfer and heat exchanger analysis, rated heat flux, and selection criteria.



Source: Edward Allen «How Buildings Work» (2005)

# Thank you for your attention!

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